

# Resonator mode analysis

Analysis of resonators

- beam sizes

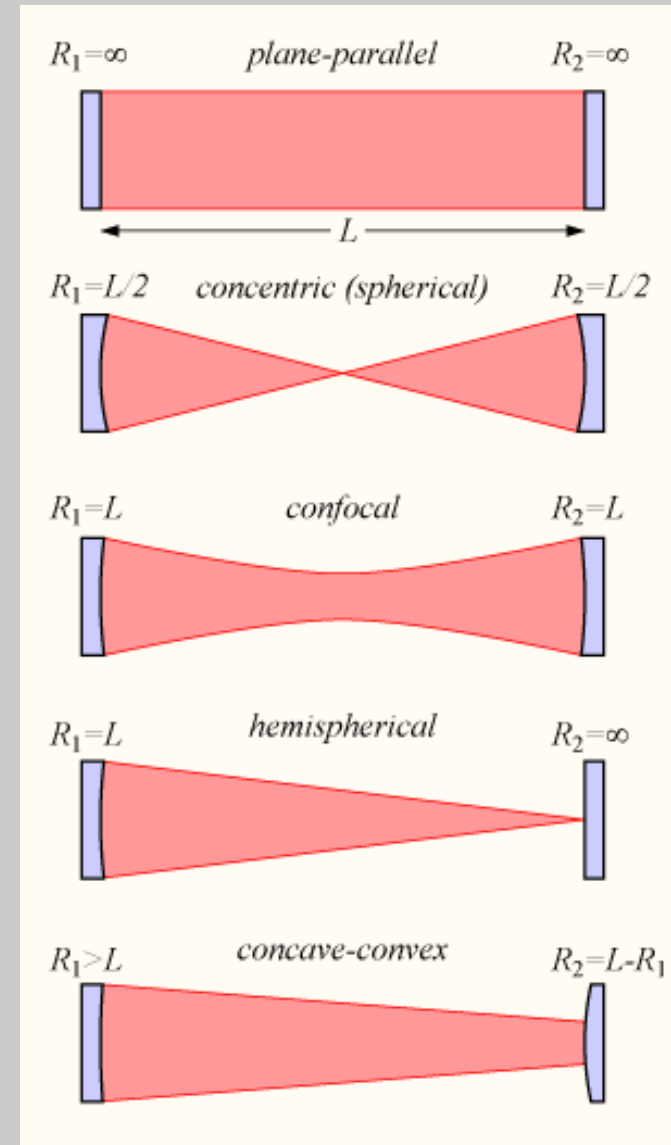
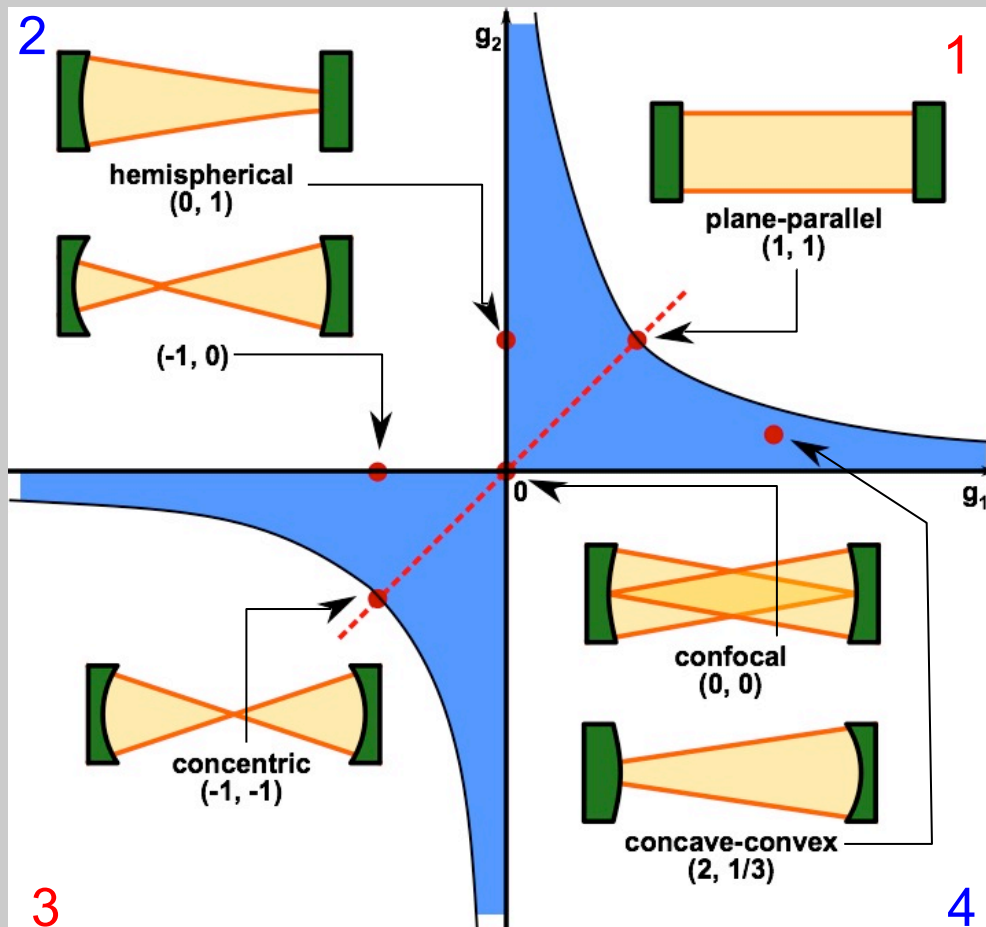
- beam waist position

Examples of resonator design

# Boundaries of stability

$$g_1 = 1 - \frac{L}{R_1} \quad g_2 = 1 - \frac{L}{R_2}$$

- Easily identified stable resonators are actually at edge of stability



# Determining beam sizes

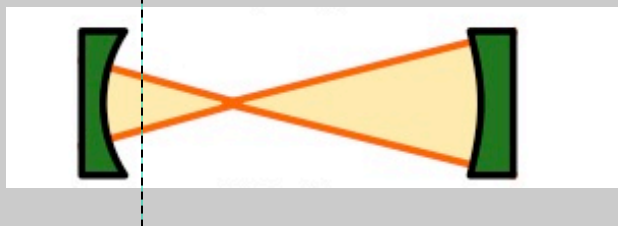
- From  $q$  parameter

- For stable mode: 
$$q_0 = \frac{(A - D)}{2C} \pm \frac{1}{2C} \sqrt{(A - D)^2 + 4BC}$$

- And  $\frac{1}{q_0} = \frac{1}{R} - i \frac{\lambda}{\pi w^2}$       Beam waist is where  $\text{Re}[1/q_0]=0$

- So  $w^2 = -\frac{\lambda}{\pi \text{Im}[q_0^{-1}]}$

- Which  $w$  is this? It is at the start/end position of the ABCD



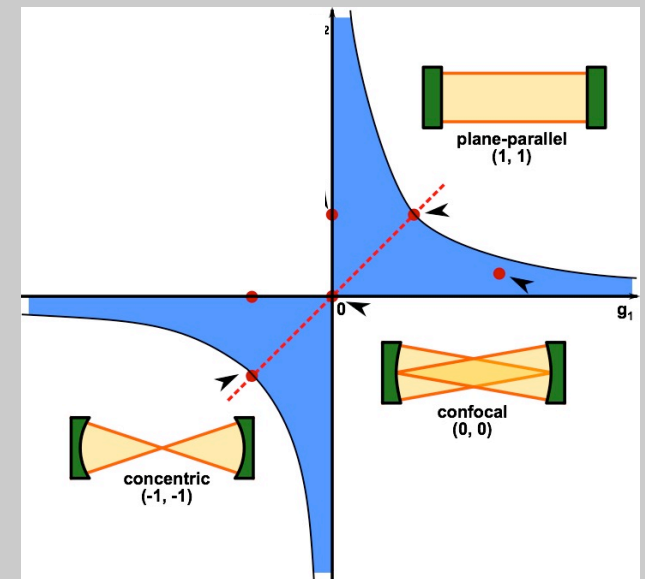
For curved end mirror, split:  
A diagram of a laser resonator with two flat mirrors. Two vertical lines represent the mirrors, with a light blue lens-like shape between them. A horizontal dashed line represents the optical axis.  
Then mode is collimated at end.

# Symmetric cavities

- At end mirror, wavefront curvature matches surface of mirror.
  - Plano end mirror: waist at mirror
  - Symmetric cavity ( $R_1=R_2$ ,  $g_1=g_2$ ): waist location at center. Can fully specify mode w/o ABCD.
- Use Gaussian beam equations:

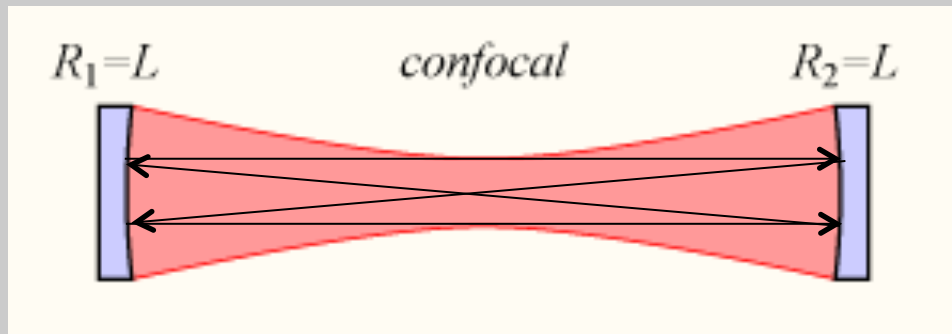
$$R = z \left( 1 + \frac{z_R^2}{z^2} \right) \rightarrow \frac{L}{2} \left( 1 + \frac{4z_R^2}{L^2} \right)$$

$$z_R = \frac{L}{2} \sqrt{\frac{2R}{L} - 1} \quad w_0 = \sqrt{\frac{\lambda L}{2\pi}} \sqrt{\frac{2R}{L} - 1}$$



# Confocal cavity

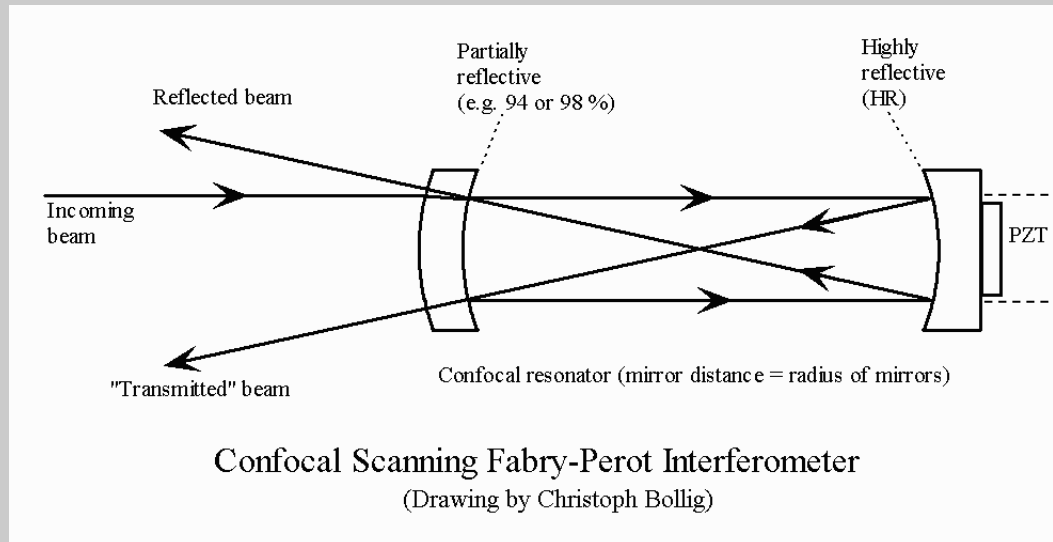
- Symmetric cavity, focal points overlap



- Cavity length is equal to the confocal parameter
- Spot size:  $w_0 = \sqrt{\frac{\lambda L}{2\pi}}$   $L = 2z_R = b$
- Confocal cavity has only ~40% variation of mode size along cavity
- Least sensitivity to angular misalignment.

# Scanning Fabry-Perot interferometer

- Confocal resonator



Transmitted beams

Look for beam overlap

See fringes: transmission through curved mirrors makes beams diverge

- Mode-matching: make input beam identical to desired output beam
  - Set initial beam size and focusing lens

# Near-planar and concentric limits

- Near-planar:  $R$  very large,  $\gg L$

$$z_R = \frac{L}{2} \sqrt{\frac{2R}{L} - 1} = \frac{L}{2} \frac{2R}{L} \sqrt{1 - \frac{L}{2R}} \approx R \left( 1 - \frac{L}{4R} \right)$$

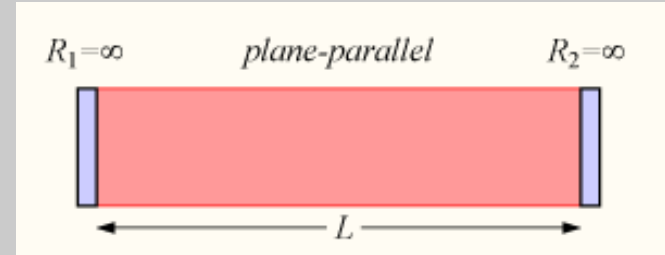
- Large, constant mode size. sensitive to angle misalignment

- Near-concentric:  $L \sim 2R$

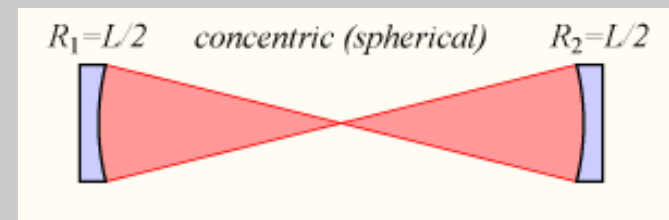
- Let  $L = 2R - \delta L$

$$z_R = \frac{L}{2} \sqrt{\frac{2R}{L} - 1} = \frac{2R - \delta L}{2} \sqrt{\frac{2R}{2R - \delta L} - 1} \approx R \sqrt{\left( 1 + \frac{\delta L}{2R} \right) - 1} \approx \sqrt{\frac{R\delta L}{2}}$$

- Small mode in center, large mode at curved mirrors



***In general, position on stability map controls mode size throughout cavity.***



# Higher-order resonator modes

- Higher-order resonator modes follow the Hermite-Gaussian (or Laguerre-Gaussian) functions

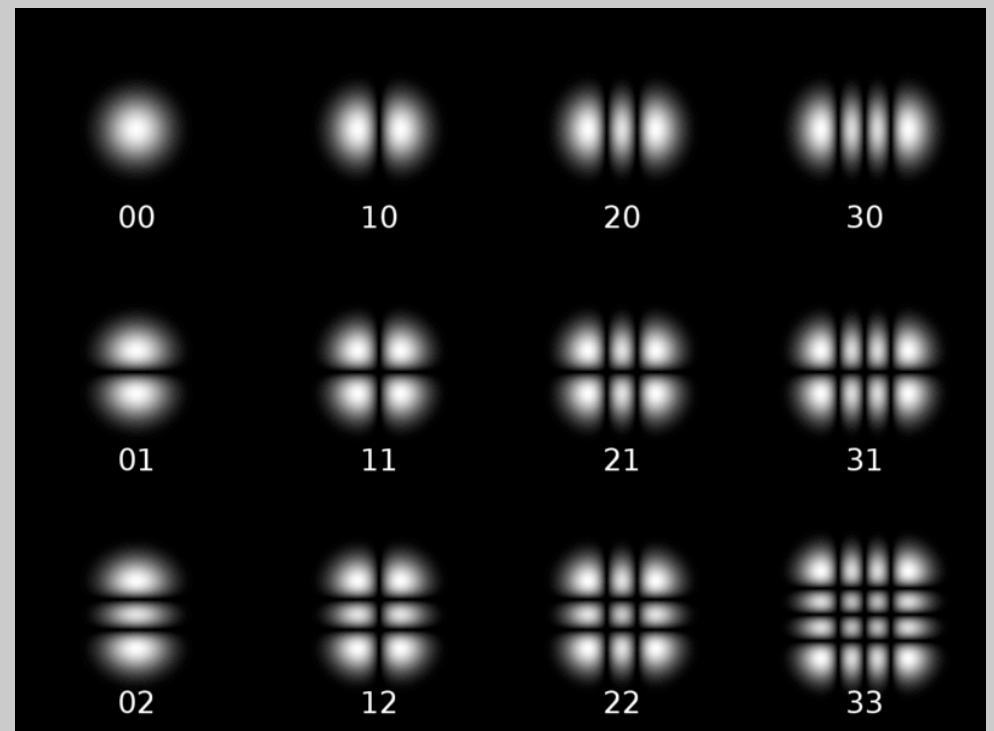
$$E(x, y, z) = A_0 e^{-i(kz - \eta_{lm}(z))} \frac{w_0}{w(z)} e^{-\frac{x^2 + y^2}{w^2(z)}} H_l \left( \frac{\sqrt{2}x}{w(z)} \right) H_m \left( \frac{\sqrt{2}y}{w(z)} \right) e^{-i \frac{k(x^2 + y^2)}{2R(z)}}$$

$$\eta_{lm} = (1 + l + m) \tan^{-1} \left( \frac{z}{z_R} \right)$$

R(z) is independent of mode order

Resonant frequencies depend on mode indices.

Extent of field is larger as mode index increases – more diffraction loss.





# Eigenvalues for high-order standing waves

- High-order modes generally have different resonant frequencies ( $n$  is longitudinal mode index)

$$\nu_{nlm} = \frac{c}{2L} \left( n + \left( \frac{1+l+m}{\pi} \right) \cos^{-1} \left( \pm \sqrt{AD} \right) \right)$$

– 2 mirror resonator:

$$\nu_{nlm} = \frac{c}{2L} \left( n + \left( \frac{1+l+m}{\pi} \right) \cos^{-1} \left( \pm \sqrt{g_1 g_2} \right) \right) \quad \begin{array}{l} + \text{ if } g_1 \text{ and } g_2 > 0 \\ - \text{ if } g_1 \text{ and } g_2 < 0 \end{array}$$

– Confocal:  $g_1 = g_2 = 0$

$$\nu_{nlm} = \frac{c}{4L} (2n + (1+l+m))$$

Even modes are degenerate  
Odd modes degenerate

## Example: 2GHz FP

- Free spectral range = 2GHz

$$\Delta\nu = \frac{c}{2L} \rightarrow L = \frac{c}{2\Delta\nu}$$

– Cavity length  $L = 7.5\text{cm}$

– Mode waist radius:  $w_0 = \sqrt{\frac{\lambda L}{2\pi}}$   
 $w_0 \sim 87\mu\text{m}$  (for 632.8nm)

– Output mode waist radius:  $\sqrt{2}w_0 = 123\mu\text{m}$

– For a general resonator, the resonant frequency is different for higher-order modes.

– For a well-aligned confocal FP, all even modes are degenerate, and odd modes are midway between TEM00 mode frequencies.

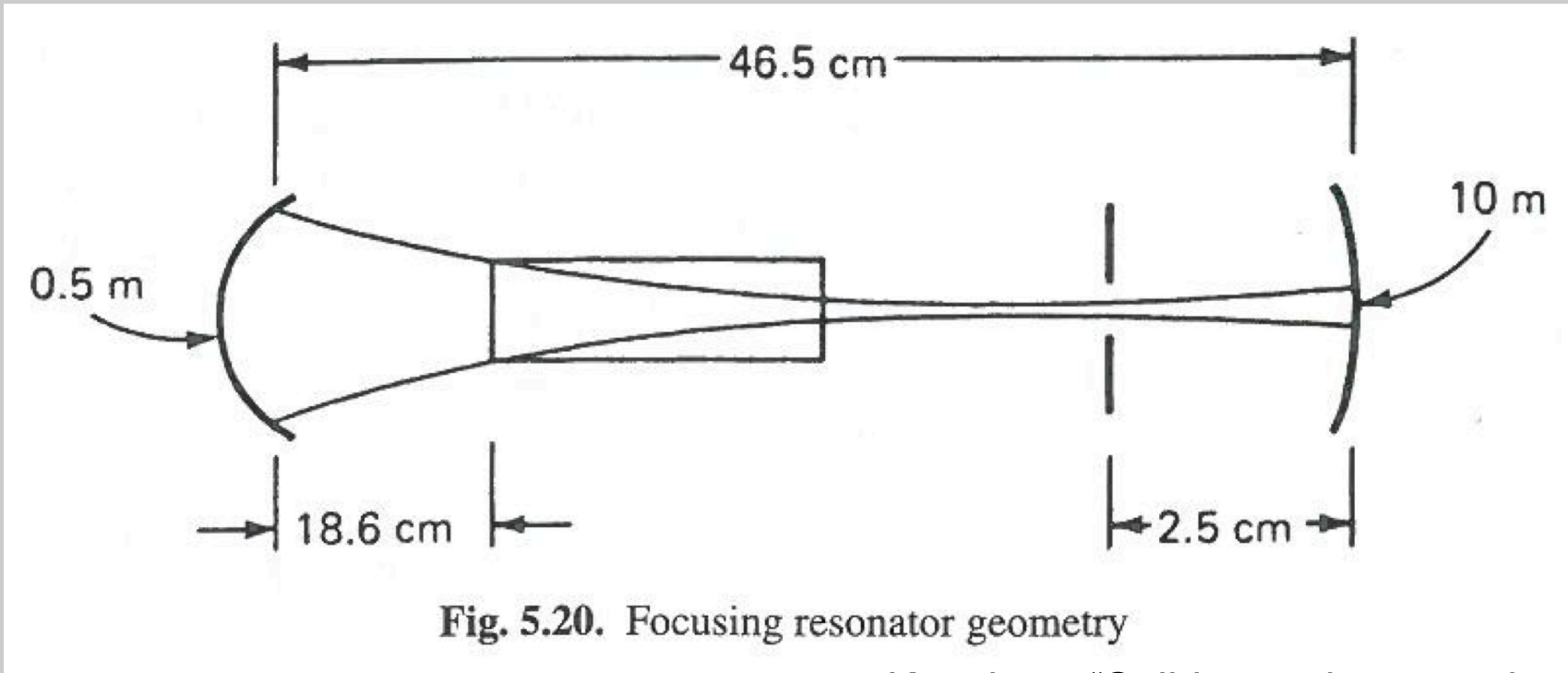
# Resonator stability analysis

- Resonators are designed under different constraints and can be optimized
- Plot a stability parameter to show stable zone(s) of operation
  - Stability condition:  $-1 < \frac{A+D}{2} < 1$
  - By convention to plot s parameter:

$$s = 1 - \left( \frac{A+D}{2} \right)^2$$

Parameter is always positive in stable zone

# Focusing resonator



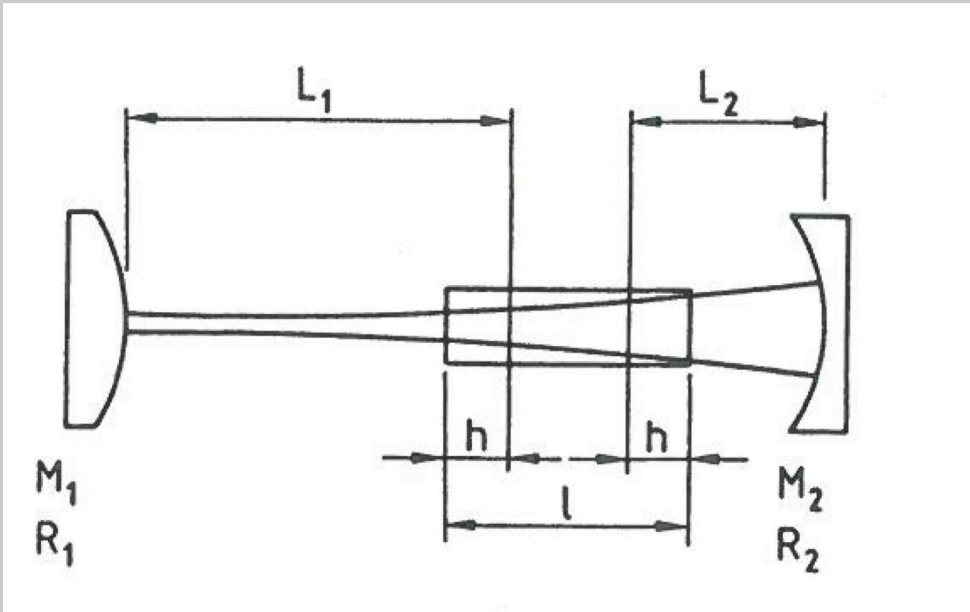
**Fig. 5.20.** Focusing resonator geometry

Koechner "Solid-state laser engineering"

Nearly hemispherical resonator

- large mode on left
- Laser rod acts as aperture to limit TEM<sub>00</sub> operation
- Second aperture to clean up beam

# Convex-concave resonator



Koechner "Solid-state laser engineering"

Shorten cavity by using a convex end mirror

Weak thermal lensing in rod

- Small spot on convex mirror
- Too intense for pulsed operation

# Internal telescope resonators

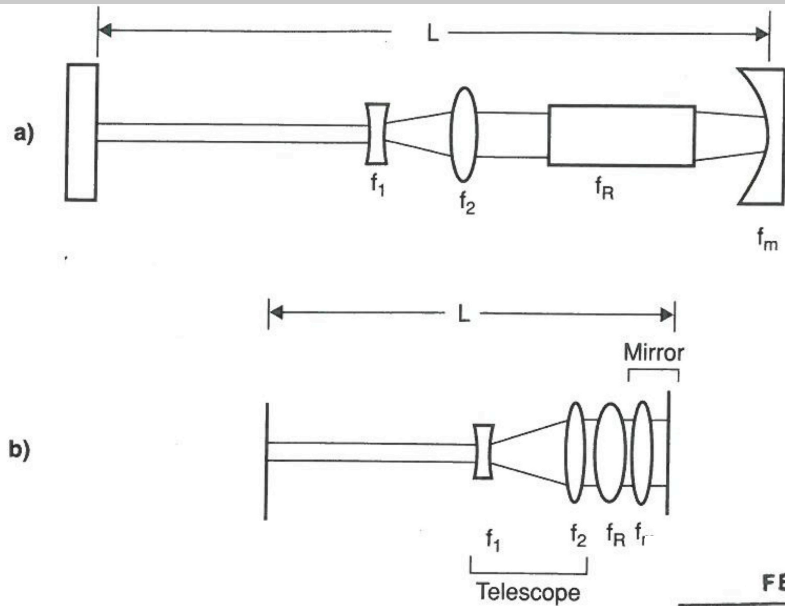
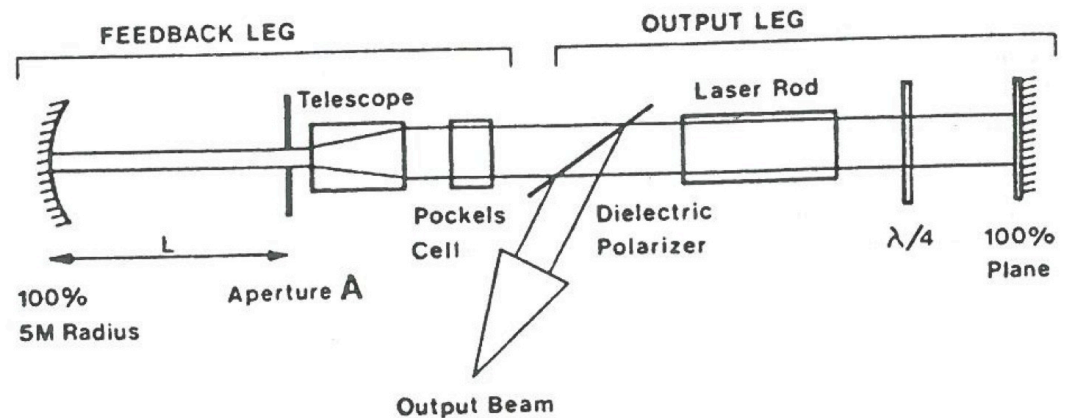


Fig. 5.27. Resonator with internal telescope, focusing laser rod, and curved mirror optical equivalent (b)

Alternatives to expand mode in gain medium while using a short resonator.



Koechner "Solid-state laser engineering"

# Mechanically-stable resonator design

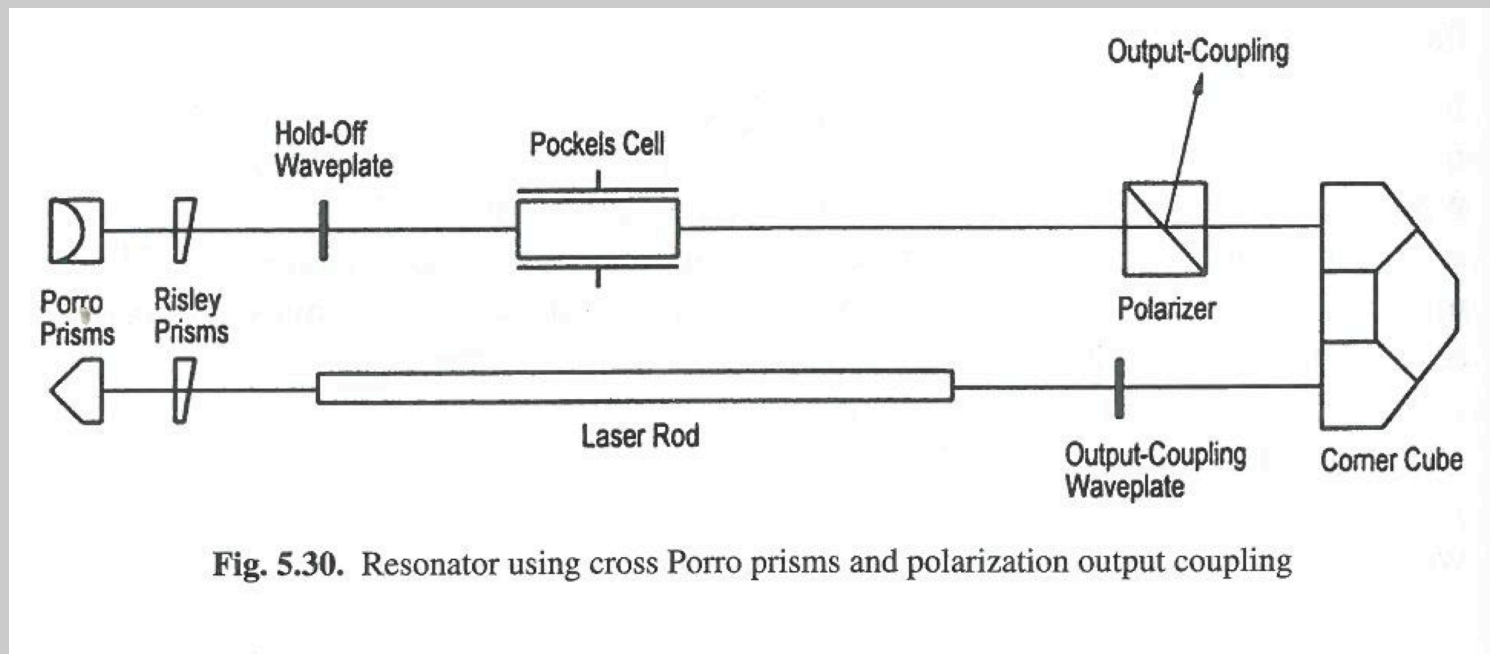
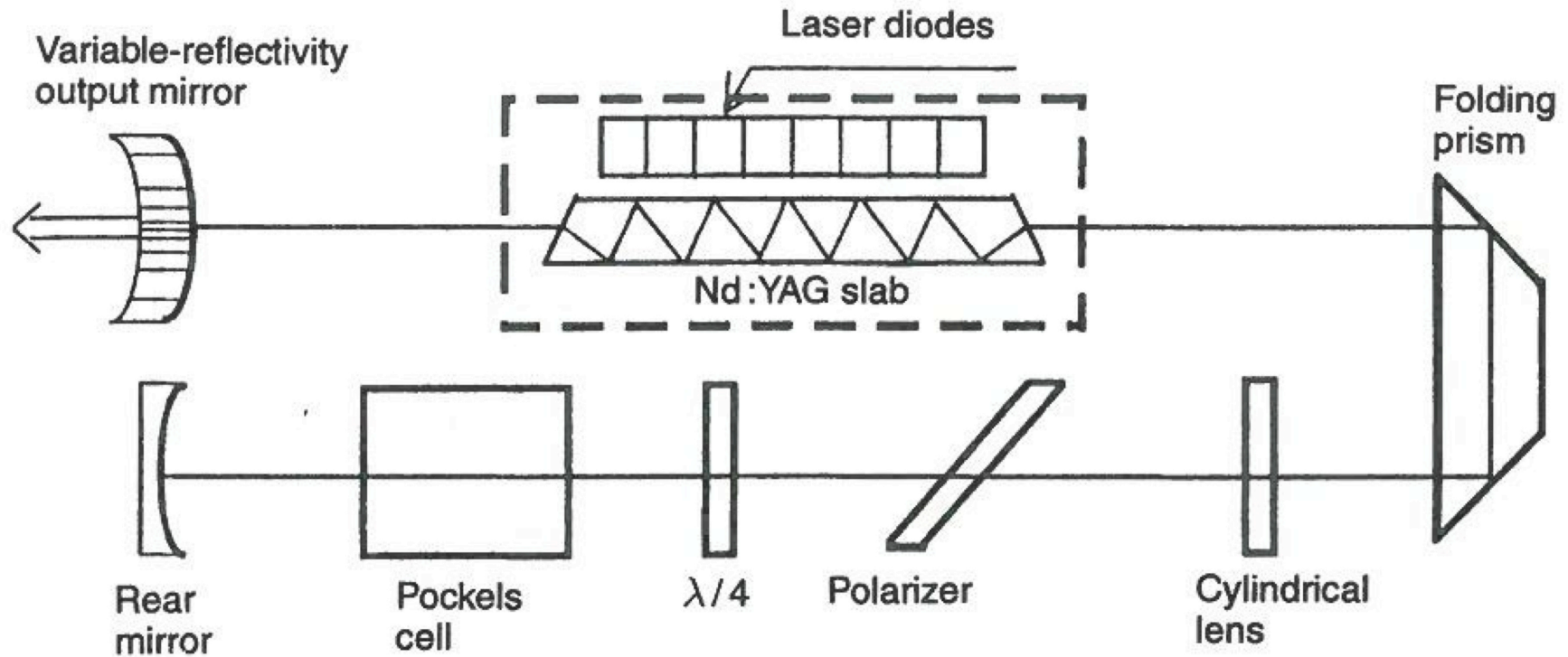


Fig. 5.30. Resonator using cross Porro prisms and polarization output coupling

Koechner “Solid-state laser engineering”

Corner cube returns beam parallel but with lateral offset.  
Porro prism does the same but only in one direction.  
Risley prisms are wedges that can be rotated to steer beams.

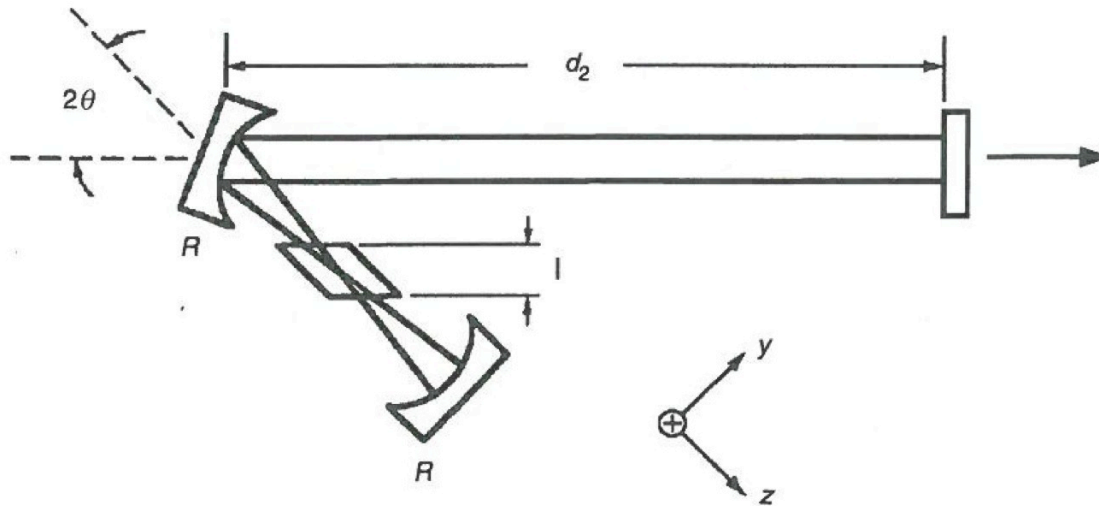
# Zig-zag slab resonator



**Fig. 5.50.** Diode-pumped Nd:YAG slab laser with positive-branch unstable resonator and variable reflectivity output coupler [5.76]



# Astigmatic compensation



**Fig. 5.29.** Astigmatic compensation of a folded resonator containing an optical element at Brewster's angle

Koechner "Solid-state laser engineering"

- Entering a tilted interface, beam propagating inside the crystal is wider
- The wider beam has a longer Rayleigh range and also travels farther to the beam waist – this leads to astigmatism
- Use tilted mirrors to compensate the astigmatism.