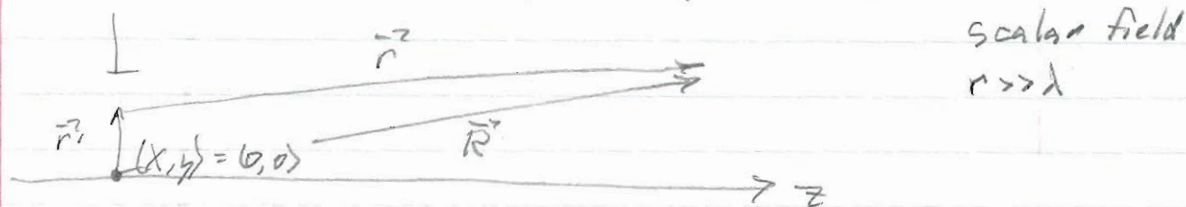


## Diffraction and the angular spectrum



$$E(\vec{R}) = \frac{1}{i\lambda} \iint E(r') \frac{e^{i k r}}{r} \cos \theta \, ds$$

spherical wave
obliquity factor.

$$U(x, y, z) = \frac{1}{i\lambda} \iint U(x', y', 0) \frac{e^{i k |\vec{R} - \vec{r}'|}}{|\vec{R} - \vec{r}'|} \frac{z}{|\vec{R} - \vec{r}'|} \, dx' dy'$$

$$r = |\vec{R} - \vec{r}'| = \sqrt{(x - x')^2 + (y - y')^2 + z^2}$$

Symbolically,

$$U(x, y, z) \sim U(x, y, 0) \otimes g(x, y, z)$$

This suggests treatment with linear systems theory  
superposition? ✓ (linear)

shift invariant ✓

can we write in transform space?

$$A(f_x, f_y, z) \sim A(f_x, f_y, 0) G(f_x, f_y, z)$$

Angular spectrum:

$$A(f_x, f_y, z=0) = \iint U(x, y, 0) e^{-i z \pi (f_x x + f_y y)} \, dx dy$$

$$= \int_{xy} \{ U(x, y, 0) \}$$

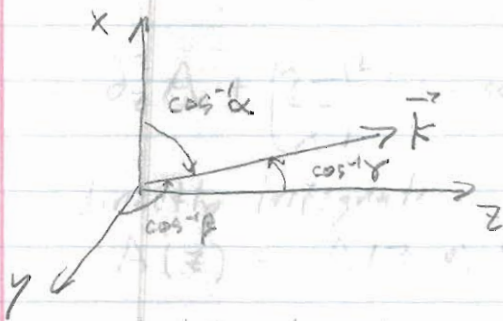
example: plane wave

$$P(x, y, z; t) = e^{i(\vec{k} \cdot \vec{r} - \omega t)} = e^{i(k_x x + k_y y + k_z z - \omega t)}$$

write  $\vec{k} = \frac{2\pi}{\lambda} (\alpha \hat{x} + \beta \hat{y} + \gamma \hat{z})$       $\lambda = \lambda_0/n$  inside medium.

$$\alpha = \hat{x} \cdot \frac{\vec{k}}{k} = \cos \theta_{xk} = \frac{k_x}{k} = \sin \theta_x$$

$\alpha, \beta, \gamma =$  "direction cosines"



$$\frac{\vec{k} \cdot \vec{k}}{n^2 k_0^2} = 1 \rightarrow \alpha^2 + \beta^2 + \gamma^2 = 1$$

put time dependence into amplitude

$$P(x, y, z) = e^{i n k_0 \gamma z} e^{i n k_0 (\alpha x + \beta y)}$$

$$\gamma = \sqrt{1 - \alpha^2 - \beta^2}$$

calculate spectrum:

$$A_P(f_x, f_y; z) = e^{i n k_0 z} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} e^{i n k_0 (\alpha x + \beta y)} \dots$$

$$\int_{-\infty}^{\infty} e^{\pm i 2\pi f_x x} dx = \delta(f_x \pm f_{x0})$$

$$f_{x0} = \frac{n k_0 \alpha}{2\pi} = \frac{\alpha}{\lambda} \quad \lambda = \lambda_0/n$$

$$f_{y0} = \beta/\lambda$$

angular spectrum:

$$A_P(f_x, f_y; z) = e^{i n k_0 z} \delta(f_x - \frac{\alpha}{\lambda}) \delta(f_y - \frac{\beta}{\lambda})$$

Propagation of the angular spectrum

$$U(x, y, z) = \mathcal{F}^{-1} \{ A(f_x, f_y, z) \} = \iint A(f_x, f_y, z) e^{i 2\pi (f_x x + f_y y) + i k_z z} df_x df_y$$

→ Helmholtz (wave) eqn:

$$\nabla^2 U + k^2 U = 0$$

$$\partial_x U = \partial_x \mathcal{F}^{-1} \{ A \} = i 2\pi f_x \mathcal{F}^{-1} \{ A \} \quad f_x = \alpha / \lambda$$

$$\rightarrow \partial_z^2 A + \left( \frac{2\pi}{\lambda} \right)^2 (1 - \alpha^2 - \beta^2) A = 0$$

directly integrate  $i \frac{2\pi}{\lambda} (1 - \alpha^2 - \beta^2)^{1/2} z$

$$A(z) = A(z=0) e^{i k_z z} = A_0 e^{i k_z z}$$

propagation in  $f_x, f_y$  space is simple:

1) calculate at  $z=0$

$$A(f_x, f_y, 0) = \mathcal{F} \{ U(x, y, 0) \}$$

2) each component propagates as

$$A(f_x, f_y, 0) \cdot \exp(i k_z (f_x, f_y) z)$$

3) transform back.

Note: if  $\alpha, \beta$  are too large,  $k_z = k_0 \sqrt{1 - \alpha^2 - \beta^2}$   
 → imaginary

waves → evanescent, don't propagate.

∴ impose bandwidth limit  $\text{circ}((\alpha^2 + \beta^2)^{1/2})$

Transfer function  $G(f_x, f_y) = e^{i 2\pi (f_x^2 + f_y^2)^{1/2} z}$   
 $\text{circ}(\lambda \sqrt{f_x^2 + f_y^2})$

Can do non-paraxial propagation with this!

## Panaxial Propagation

- for small angles, we can approximate  $\sqrt{\alpha^2 + \beta^2}$  in propagator.
- equivalent to approx  $r = \sqrt{(x-x')^2 + (y-y')^2 + z^2}$

back to diffraction integral:

$$U(x, y, z) = \frac{1}{i\lambda} \iint U(x', y') \frac{e^{ikr}}{r} \cos \theta \, dx' dy'$$

panaxial approximation

amplitude term  $\frac{\cos \theta}{r} = \frac{z}{r^2} \approx \frac{1}{z}$

phase:  $kr = \frac{2\pi n}{\lambda_0} z \sqrt{1 + \left(\frac{x-x'}{z}\right)^2 + \left(\frac{y-y'}{z}\right)^2}$

$$\approx kz \left( 1 + \frac{(x-x')^2}{2z^2} + \frac{(y-y')^2}{2z^2} \right)$$

$$= k \left( z + \frac{x^2 + y^2}{2z} - \frac{xx' + yy'}{z} + \frac{x'^2 + y'^2}{2z} \right)$$

note  $\frac{x}{z} \approx \sin \theta_x$  so  $\frac{x}{z} \frac{1}{\lambda} \approx f_x$

$$U(x, y, z) = \frac{1}{i\lambda z} e^{ikz} e^{ik(x^2+y^2)/2z} \iint U(x', y') e^{-i2z(f_x x' + f_y y')} e^{i\frac{k}{2z}(x'^2+y'^2)} \, dx' dy'$$

$$= \frac{1}{i\lambda z} e^{ikz} e^{ik(x^2+y^2)/2z} \iint_{x', y'} \left\{ U(x', y') e^{i\frac{k}{2z}(x'^2+y'^2)} \right\} \, dx' dy'$$

= Fresnel propagation

Fraunhofer propagation: drop quadratic phase factor.  
 $\rightarrow$  Fourier transform!

when is  $e^{i\frac{k}{2z}(x'^2+y'^2)} \approx 1$  ?

Far-field approximation

when is  $e^{i k(x'^2 + y'^2)/2z} \approx 1$  ?

let input be bounded by  $x', y' < a$ ,  $z \rightarrow L$

$e^{i k a^2/2L} \approx 1$  if  $\frac{a^2}{L\lambda} \ll 1$

$$F = \frac{a^2}{L\lambda} = \text{Fresnel \#}$$



$F \ll 1 \rightarrow$  Fraunhofer

recall for Gaussian beams:

$$z_R = \frac{\pi w_0^2}{\lambda}$$

$$\text{so } \frac{\pi a^2/\lambda}{L} \sim \frac{z_R}{L\pi}$$

# Fraunhofer diffraction

From paraxial analysis

$$U(x, y, z) = \frac{e^{ikz}}{i\lambda z} e^{ik \frac{(x^2+y^2)}{2z}} \iint U(x', y') e^{\frac{ik}{2z}(x'^2+y'^2)} e^{-i2\pi(f_x x + f_y y)} dx' dy'$$

if input is spatially localized to a radius  $a$ , then we can drop quadratic phase term inside integral:

$$\max\left(\frac{k(x'^2+y'^2)}{2z}\right) \sim \frac{ka^2}{2z}$$

$$\text{if } \frac{ka^2}{2z} \ll \pi \text{ or } F = \frac{a^2}{z\lambda} \ll 1$$

Fresnel number.

dropping quadratic phase  $\rightarrow$  Fraunhofer diffraction  
 $\rightarrow$  Fourier transform!

discuss terms in expression:

$$1) \iint U(x', y') e^{-i2\pi(f_x x + f_y y)} dx' dy' = \int_{x'} \int_{y'} \{U(x', y')\}$$

$$f_x = \frac{x}{z\lambda} = \frac{\sin\theta}{\lambda} \quad f_y = \frac{y}{z\lambda} = \frac{\sin\theta}{\lambda}$$

do FT w.r.t.  $x', y' \rightarrow U(f_x, f_y) \rightarrow U(x, y, z)$

note wavelength +  $z$  scaling of pattern.

$$\lambda \text{ is inside medium} = \lambda_0/n$$

2.  $e^{\frac{iK}{2z}(x^2+y^2)}$  = spherical wavefront  
FT of input field will have phase that will modify this

3.  $e^{ikz}$  = overall propagation phase.

4.  $\frac{1}{i\lambda z}$   $\rightarrow$  intensity varies as  $\frac{1}{\lambda^2 z^2}$   
more diffraction with long  $\lambda \rightarrow$  bigger spread.  
 $\rightarrow$  less intensity.

Fraunhofer diffraction examples.

$$U(x, y, z) = \frac{e^{ikz}}{i\lambda z} e^{i\frac{k}{2z}(x^2+y^2)} \int_{x'y'} \{ U(x', y') \}$$

$$A(f_x, f_y)$$

$$f_x = \frac{x}{z\lambda}$$

$$f_y = \frac{y}{z\lambda}$$

$U(x', y')$  is field leaving plane  $z=0$

$$U_z(x', y') = U_i(x, y, 0) \cdot t_A(x, y)$$

transmitted  
field

input  
field

aperture plane  
transmission fn.

(complex)

(complex)

note:

$$A_z(f_x, f_y) = A_i(f_x, f_y) \otimes T(f_x, f_y)$$

i) rectangular aperture, uniform plane wave illumination  
normal incidence

$$U_t(x', y') = E_0 \underbrace{\text{rect}(x/a)}_{U_i} \underbrace{\text{rect}(y/b)}_{t_A}$$

$$A(f_x, f_y) = ab \text{sinc}(\pi f_x a) \text{sinc}(\pi f_y b)$$

$$U(x, y, z) = \frac{E_0 e^{ikz}}{i\lambda z} e^{i\frac{k}{2z}(x^2+y^2)} \cdot ab \text{sinc}\left(\frac{\pi a}{z\lambda} x\right) \text{sinc}\left(\frac{\pi b}{z\lambda} y\right)$$

Full width: 1st zero at  $x = \frac{\lambda z}{a}$  where  $\sin(\pi) = 0$

$$FW = 2\lambda z/a \quad \text{diffraction } \frac{1}{2} \text{ angle } \theta \sim \frac{x_{FW}}{z}$$

$$\theta \sim \frac{\lambda}{a}$$

$$I(x, y, z) \propto \frac{E_0^2}{\lambda^2 z^2} a^2 b^2 \text{sinc}^2(\ ) \text{sinc}^2(\ )$$



2) plane wave input, angle of incidence  $\theta_{x0}$

$$U_{in} = E_0 e^{i k_0 (\sin \theta_{x0}) x'}$$

by shift theorem,  $\int \{ e^{i z \pi f_{x0} x} g(x) \} = G(f_x - f_{x0})$

identity  $2\pi f_{x0} = k_0 \sin \theta_{x0} \rightarrow f_{x0} = \frac{\sin \theta_{x0}}{\lambda}$

since  $f_x = \frac{x}{\lambda z} \rightarrow \text{sinc}(\pi (f_x - f_{x0}) a)$

$$= \text{sinc} \left( \frac{\pi a}{\lambda z} x - \frac{\sin \theta_{x0} \cdot \pi a}{\lambda} \right)$$

$$\frac{\pi a}{\lambda z} (x - z \sin \theta_{x0})$$

geometrically, expect shift by  $z \tan \theta_{x0} = z \frac{\sin \theta_{x0}}{\cos \theta_{x0}}$   
small angle

3) double slit, width  $a$ , separation  $d$   
 normal incidence

$$t_A(x, y) = \left[ \text{rect} \left( \frac{x-d/2}{a} \right) + \text{rect} \left( \frac{x+d/2}{a} \right) \right] \text{rect} \left( \frac{y}{b} \right)$$

shift  $A(f_x) = a e^{-2\pi f_x (d/2)} \text{sinc}(\pi f_x a) + a e^{+2\pi f_x (d/2)} \text{sinc}(\pi f_x a)$

$$= 2a \cos(\pi f_x d) \text{sinc}(\pi f_x a)$$

conv:  $t_A(x, y) = \text{rect} \left( \frac{x}{a} \right) \otimes \left( \delta(x-d/2) + \delta(x+d/2) \right)$

$$A(f_x) = a \text{sinc}(\pi f_x a) \cdot \left( e^{i\pi f_x d/2} + e^{-i\pi f_x d/2} \right)$$


$$2 \cos(\pi f_x d)$$

fringe spacing:  $\pi \frac{x_0}{\lambda z} d = 2\pi \quad x_0 = \frac{2\lambda z}{d}$

4) transmission spatial light modulator. SLM

programm  $n(x)$   
 modulation  $e^{i \frac{2\pi}{\lambda_0} n(x) \delta z}$

linear phase ramp:

$$n(x) = n_{\max} x/x_0$$


$$t_A(x) = e^{i \left( \frac{2\pi n_{\max} \delta z}{\lambda_0 x_0} \right) x}$$

$$\underbrace{2\pi f_{x0} x}_{2\pi f_{x0} x} \quad f_{x0} = \frac{n_{\max} \delta z}{\lambda_0 x_0} = \frac{\sin \theta_{x0}}{\lambda_0}$$

steers beam by  $\theta_{x0}$

note: typically we can get only few  $\cdot \pi$  delay.  
 $\therefore$  wrap every  $2\pi$

5) transition from  $n_1$  to  $n_2$ , surface normal  $\parallel z$



incident wave  $E_0 e^{ik_x x} = E_0 e^{ik_0 n_1 \sin \theta_1 x}$

incident angular spect:  $E_0 \delta(f_x - \frac{k_0 n_1 \sin \theta_1}{2\pi}) \delta(f_y)$

where  $f_x = x/\lambda$   $\lambda$  is inside medium =  $\lambda_0/n_1$

starting  $f_{x1} = \frac{n_1 \sin \theta_1}{\lambda_0}$


by Snell  $f_{x2} = \frac{n_2 \sin \theta_2}{\lambda_0} = f_{x1}$

$\therefore A(f_x, f_y)$  is unchanged when crossing surface  $\perp z$

But an angled surface  $\rightarrow$  change in direction, shift in  $f_x$

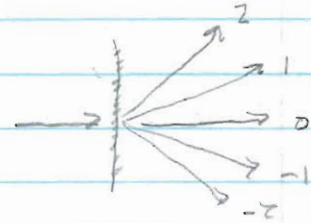
e.g. thin wedge  $d(x) = (x - x_0) \cdot \delta$

$\rightarrow$  phase  $\frac{2\pi n d(x)}{\lambda_0} = \frac{2\pi n (x - x_0) \delta}{\lambda_0} \Rightarrow f_{x0} = \frac{n \delta}{\lambda_0}$  as in SLM example.

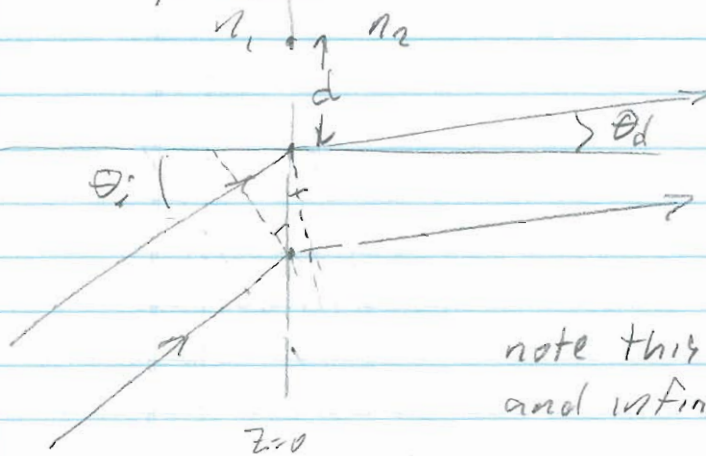


## Diffraction gratings

- used for angular dispersion
- transmission
- reflection



## Grating equation



$$\Delta(n\lambda) = n_1 d \sin \theta_i - n_2 d \sin \theta_d = m\lambda$$

$$\rightarrow n_2 \sin \theta_d = \frac{m\lambda}{d} + n_1 \sin \theta_i$$

note this assumes point sources and infinite plane waves

in spatial frequency variables:

$$f_{xd} = \frac{m}{d} + f_{xi}$$

in  $k_x$ 's  $k_{xd} = k_g + k_{xi}$  grating has a  $k$  contrib.

reflection from facet - normal incidence



change direction by  $2\alpha$   
 $\rightarrow e^{ik \sin 2\alpha x}$

facet width  $a$   $\text{rect}(x/a)$

infinite array, spacing  $d$   $\text{comb}(x/d)$

overall edge of grating  $\text{rect}(x/D)$

# Blazed diffraction grating, reflection



single element.



phase from tilt,  $e^{i k_0 x \sin \alpha}$ .  
look at relative phase.

$\therefore$  each element is  $\text{rect}(x/a) e^{i k_0 \cdot 2 \sin \alpha x}$

array:  $\text{rect}(x/D) \text{comb}(x/d)$

full grating:  $[\text{rect}(x/D) \text{comb}(x/d)] \otimes [\text{rect}(x/a) e^{i k_0 2 \sin \alpha x}]$

groove:  $\rightarrow a \text{sinc}(\pi a (f_x - \frac{2k_0 \sin \alpha}{2\pi}))$

$$= a \text{sinc}(\pi a (\frac{x}{\lambda z} - \frac{2 \sin \alpha}{\lambda}))$$

array:  $D \text{sinc}(\pi f_x D) \otimes \frac{1}{d} \text{comb}(f_x d)$

full grating: product

$$[D \text{sinc}(\pi f_x D) \otimes \frac{1}{d} \text{comb}(f_x d)] a \text{sinc}(\frac{\pi a}{\lambda z} (x - 2z \sin \alpha))$$

interpretation:

smallest feature  $\text{sinc} \left( \frac{\pi D}{\lambda z} x \right) \rightarrow$  lineshape

width determined by size of grating.

$$D = Nd$$

diffraction orders

$$\text{comb}(fxd) \rightarrow \sum \delta(fx - m/d)$$

$$\text{peaks at } \frac{x}{\lambda z} = m/d$$

$$x/z \approx \sin \theta_d \rightarrow m\lambda = d \sin \theta_d$$

$$m = 0, \pm 1, \pm 2, \dots$$

groove shape  $\rightarrow$  envelope on orders.

if  $\alpha = 0$ , max at  $x = 0$ , zero order.

can adjust peak:

$$x_{\text{pk}} = 2z \sin \alpha$$

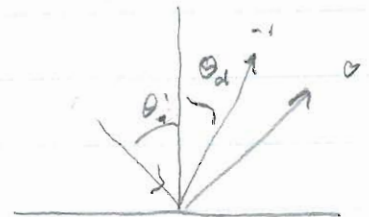
$$\text{for first order, } \rightarrow 2z \sin \alpha = \sin \theta_d$$

Non-normal incidence  $i k_0 \sin \theta_i \cdot x$

$$E_{\text{in}} = E_0 e$$

shift all by  $x' = z \sin \theta_i$

$$\rightarrow m\lambda = d (\sin \theta_d - \sin \theta_i)$$



Littrow angle:  $\theta_d = -\theta_i$ ,  $m = -1$

"blaze wavelength" peak into  $-1$  order at Littrow for  $\lambda_{\text{blaze}}$