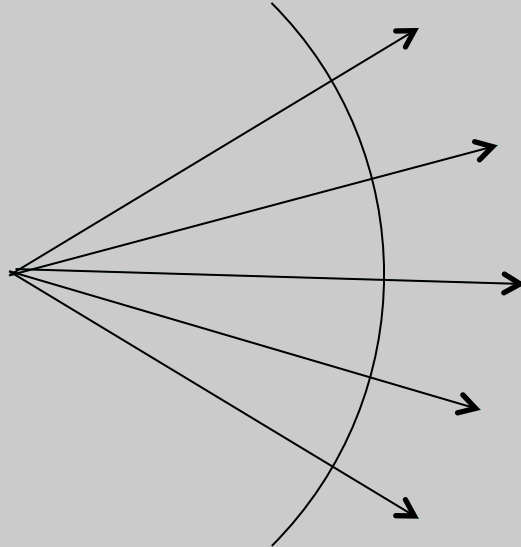


Curved wavefronts

- Rays are directed normal to surfaces of constant phase
 - These surfaces are the wavefronts
 - Radius of curvature is approximately at the focal point



- Spherical waves are solutions to the wave equation (away from $r = 0$)

$$\nabla^2 E + \frac{n^2 \omega^2}{c^2} E = 0$$

$$E \propto \frac{1}{r} e^{i(\pm kr - \omega t)}$$
$$I \propto \frac{1}{r^2}$$

Scalar r
+ outward
- inward

Paraxial approximations

- For **rays**, paraxial = small angle to optical axis
 - Ray slope: $\tan \theta \approx \theta$

- For **spherical waves** where power is directed forward:

$$e^{ikr} = \exp\left[ik\sqrt{x^2 + y^2 + z^2}\right]$$

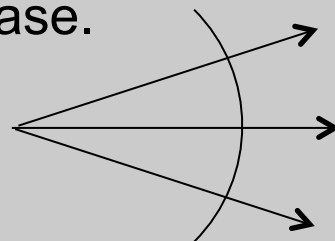
$$k\sqrt{x^2 + y^2 + z^2} = kz\sqrt{1 + \frac{x^2 + y^2}{z^2}} \approx kz\left(1 + \frac{x^2 + y^2}{2z^2}\right) \quad \text{Expanding to 1st order}$$

$$e^{i(kr - \omega t)} \rightarrow e^{ikz} \exp\left[i\left(k\frac{x^2 + y^2}{2z} - \omega t\right)\right] \quad z \text{ is radius of curvature}$$

Wavefront = surface of constant phase

For $x, y > 0$, t must increase.

Wave is diverging:



$$k\frac{x^2 + y^2}{2z} = \omega t$$

3D wave propagation

$$\nabla^2 \mathbf{E} - \frac{n_j^2}{c^2} \frac{\partial^2}{\partial t^2} \mathbf{E} = \frac{\partial^2}{\partial z^2} \mathbf{E} + \nabla_{\perp}^2 \mathbf{E} - \frac{n(\mathbf{r})^2}{c^2} \frac{\partial^2}{\partial t^2} \mathbf{E} = 0$$

- Note:

$$\nabla_{\perp}^2 = \partial_x^2 + \partial_y^2$$

$$\nabla_{\perp}^2 = \frac{1}{r} \partial_r (r \partial_r) + \frac{1}{r^2} \partial_{\phi}^2$$

- All linear propagation effects are included in LHS: diffraction, interference, focusing...
 - Previously, we assumed plane waves where transverse derivatives are zero.
- More general examples:
 - Gaussian beams (including high-order)
 - Waveguides
 - Arbitrary propagation
 - Can determine discrete solutions to linear equation (e.g. Gaussian modes, waveguide modes), then express fields in terms of those solutions.

Diffractive propagation

- Huygens' principle:
 - Represent a plane wave as a superposition of source points emitting spherical waves
- Integral representation:

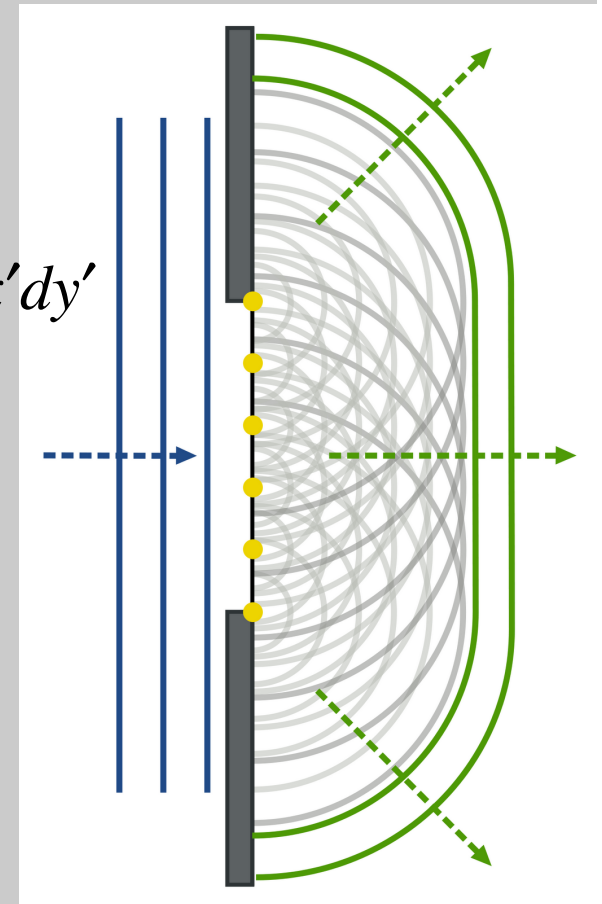
$$E(x, y, z) = \frac{i}{\lambda} \iint E(x', y', z') \frac{\exp[-ik|\mathbf{r} - \mathbf{r}'|]}{|\mathbf{r} - \mathbf{r}'|} \cos\theta dx' dy'$$

Field at
input plane

Spherical
wavelet

Inclination
factor

This is essentially a convolution of the complex input field with the spherical wavelets, which are the Green's function for the wave equation



Paraxial, slowly-varying approximations

- Assume

- waves are forward-propagating:

$$\mathbf{E}(\mathbf{r}, t) = \mathbf{A}(\mathbf{r}) e^{i(kz - \omega_0 t)} + \text{c.c.}$$

- Refractive index is isotropic

$$\frac{\partial^2}{\partial z^2} \mathbf{A} + 2ik \frac{\partial}{\partial z} \mathbf{A} - k^2 \mathbf{A} + \nabla_{\perp}^2 \mathbf{A} + \frac{n^2 \omega_0^2}{c^2} \mathbf{A} = 0$$

- Fast oscillating carrier terms cancel (blue)

- Slowly-varying envelope: compare red terms

- Drop 2nd order deriv if $\frac{2\pi}{\lambda} \frac{1}{L} A \gg \frac{1}{L^2} A$

- This ignores:

- Changes in z as fast as the wavelength
- Counterpropagating waves

$$2ik \frac{\partial}{\partial z} \mathbf{A} + \nabla_{\perp}^2 \mathbf{A} = 0$$

Fresnel diffraction integral

- Fresnel approximation (near field)
 - Expand the spherical wave in paraxial approximation (in exponential)
 - Let denominator be $|\mathbf{r} - \mathbf{r}'| \sim z - z' = L \quad \cos\theta \simeq 1$
 - Input field: $E(x', y', z') = u(x', y', z') e^{-ik(z-z')}$

$$u(x, y, z) = \frac{i}{\lambda L} \iint u(x', y', z') \exp\left[-ik \frac{(x-x')^2 + (y-y')^2}{2L}\right] dx' dy'$$

$$u(x, y, z) = \frac{i}{\lambda L} e^{-ik \frac{x^2+y^2}{2L}} \iint u(x', y', z') e^{-ik \frac{x'^2+y'^2}{2L}} e^{-i \frac{k}{L}(xx'+yy')} dx' dy'$$

Fraunhofer diffraction integral

$$u(x, y, z) = \frac{i}{\lambda L} e^{-ik \frac{x^2 + y^2}{2L}} \iint u(x', y', z') e^{-ik \frac{x'^2 + y'^2}{2L}} e^{-i \frac{k}{L} (xx' + yy')} dx' dy'$$

- In the “far field”, we approximate the sum of paraxial spherical waves as a sum of plane waves
 - Assume field in input plane is confined to a radius a
 - If $\frac{ka^2}{2L} = \frac{\pi a^2}{\lambda} \frac{1}{L} \ll 1$ then we drop quadratic phases.

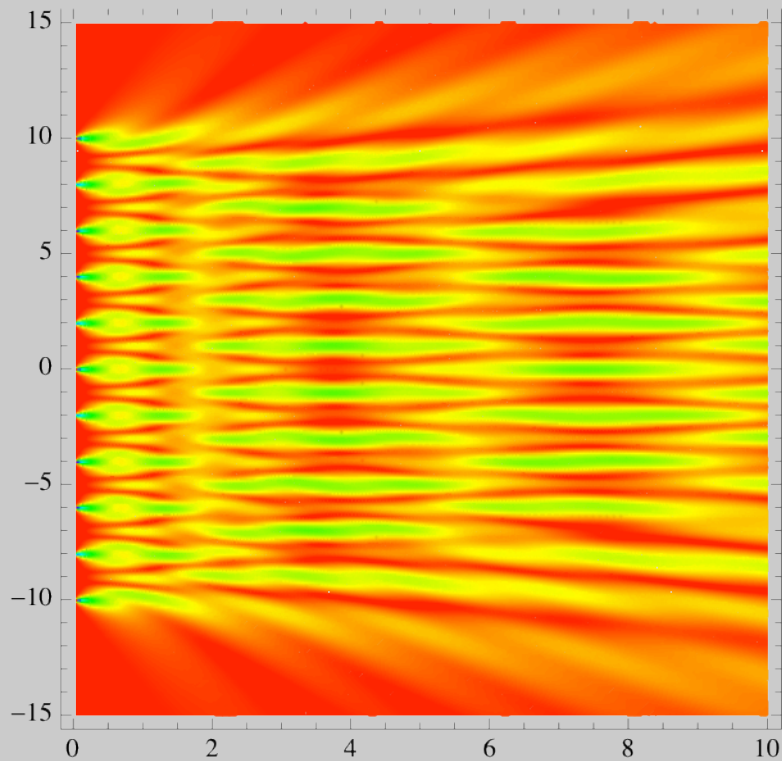
$$u(x, y, z) = \frac{i}{\lambda L} \iint u(x', y', z') \exp \left[-i \left(\frac{kx}{L} x' + \frac{ky}{L} y' \right) \right] dx' dy'$$

- Result: far field is a Fourier transform of the input field
- “spatial frequencies” $\beta_x = k \frac{x}{L} = k \sin \theta_x$ $\beta_y = k \frac{y}{L} = k \sin \theta_y$

Example: sum of dipole radiators

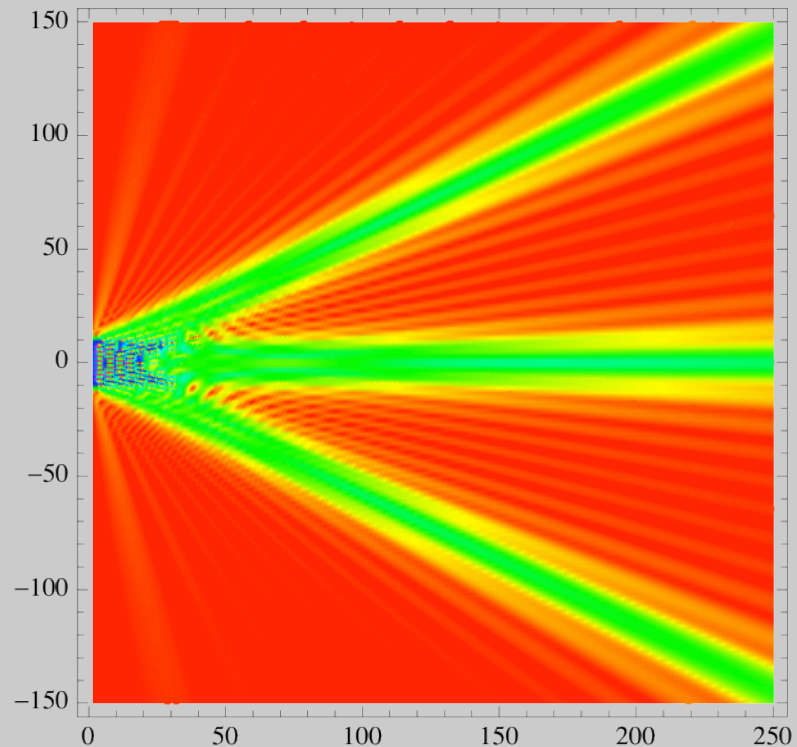
- Add fields from 10 individual sources

Near field



Talbot fringes

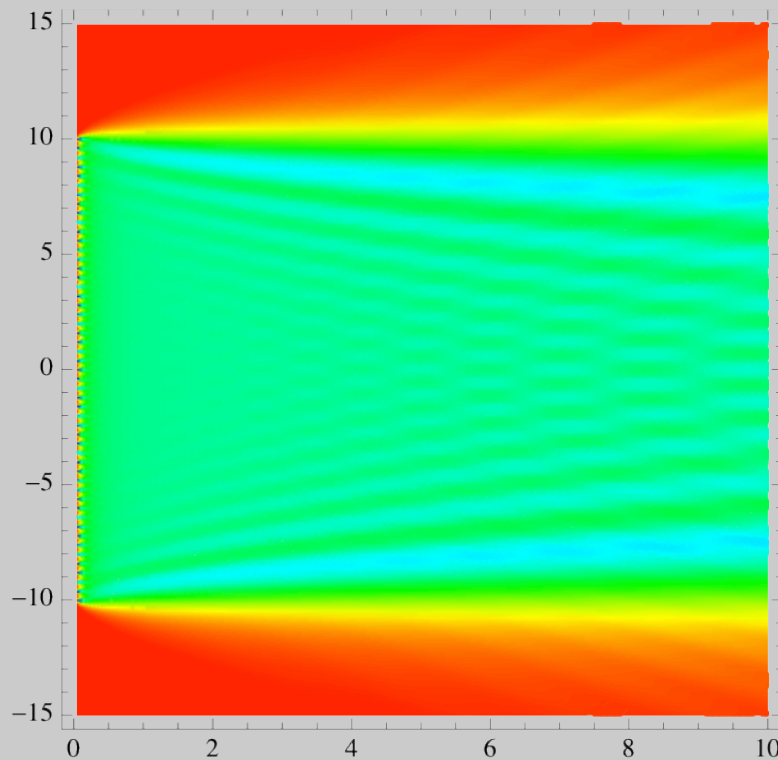
far field



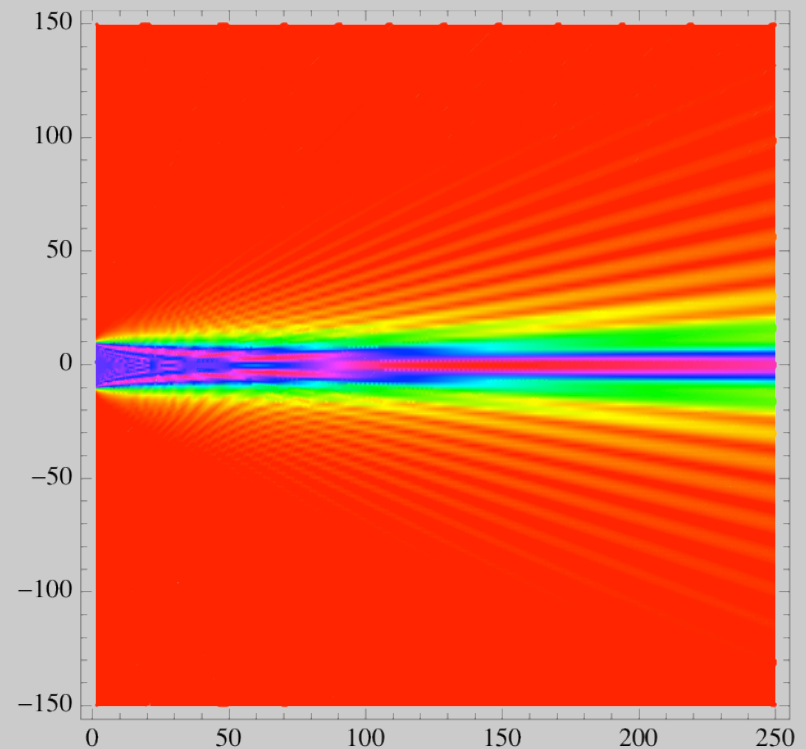
Diffraction grating

High-density of radiators

- Combine 50 sources over same distance



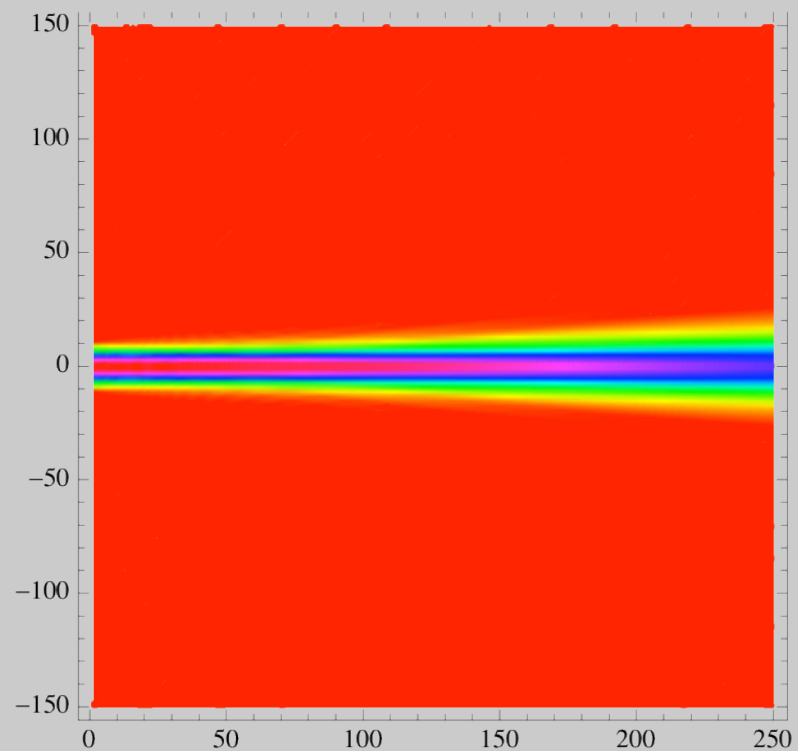
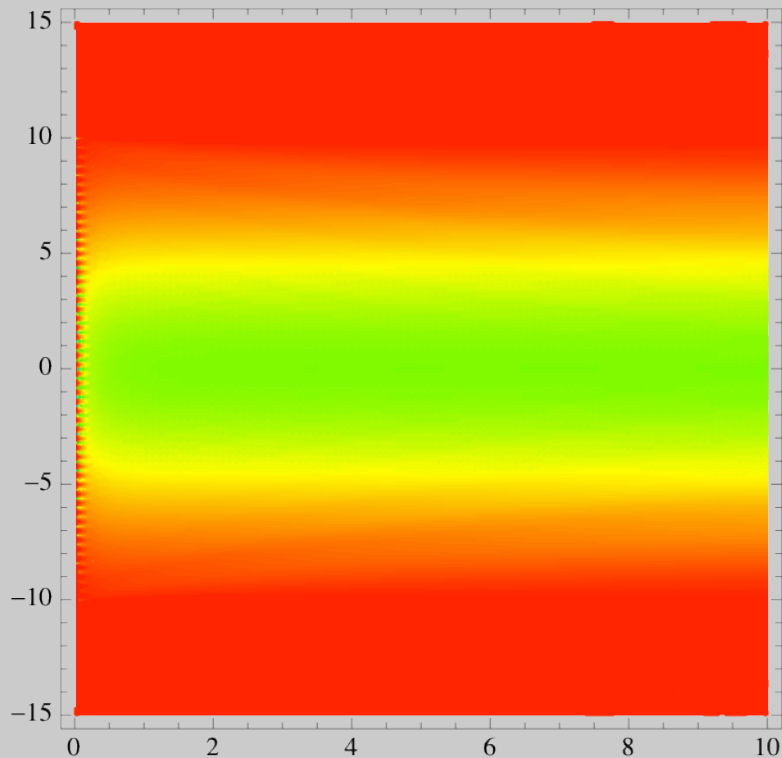
Fresnel zone shows shadow boundary, diffraction fringes



Far field evolves more like a beam, with single-slit diffraction.

High density of radiators, Gaussian envelope

- Gaussian amplitude envelope eliminates diffraction fringes



Beam smoothly spreads
out with distance

Gaussian beam solution to wave equation

- Use Fresnel integral to propagate a Gaussian beam

$$u(x, y, z) = \frac{i}{\lambda L} e^{-ik \frac{x^2+y^2}{2L}} \iint e^{-\frac{x'^2+y'^2}{w^2}} e^{-ik \frac{x'^2+y'^2}{2L}} e^{-i(\beta_x x' + \beta_y y')} dx' dy'$$

- Combine quadratic terms in exponent:

$$\left(\frac{1}{w^2} + i \frac{k}{2L} \right) = i \frac{k}{2} \left(\frac{1}{L} - i \frac{2}{kw^2} \right) = i \frac{k}{2q}$$

- Now integral is a F.T. of a complex Gaussian=Gaussian

$$u(x, y, z) = \frac{i}{\lambda L} e^{-ik \frac{x^2+y^2}{2L}} \iint e^{-ik \frac{x'^2+y'^2}{2q}} e^{-i(\beta_x x' + \beta_y y')} dx' dy'$$

Standard form of Gaussian beam equations

$$E(r, z, t) = A_0 e^{-i(kz - \omega t)} \frac{w_0}{w(z)} e^{-\frac{r^2}{w^2(z)}} e^{-i\frac{kr^2}{2R(z)}} e^{i\eta(z)}$$

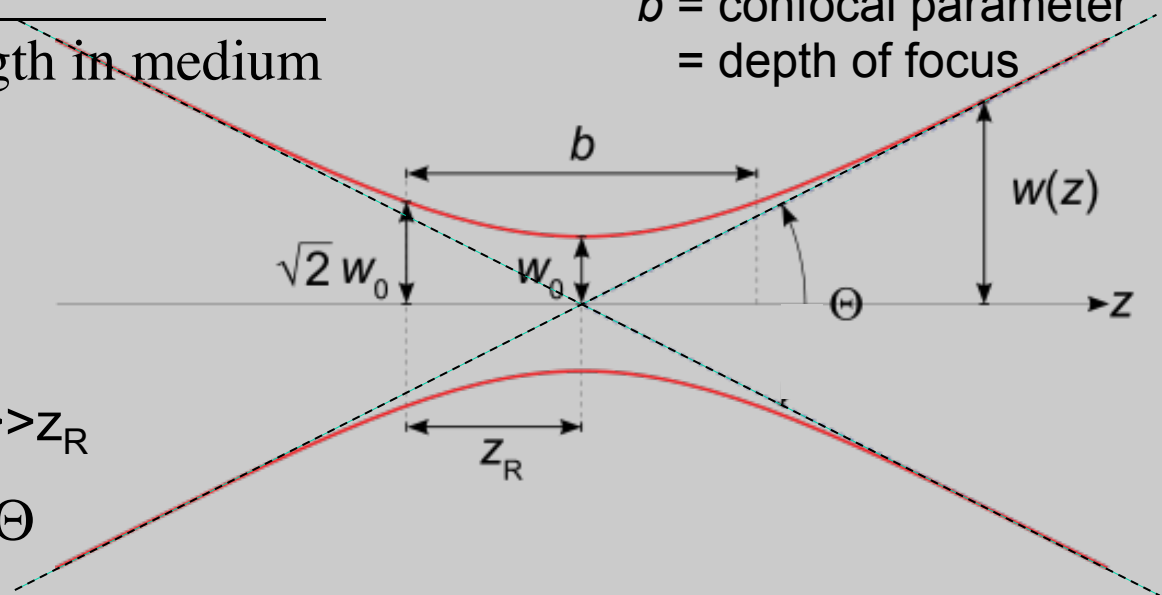
Beam maintains a Gaussian profile as it propagates

- beam radius that varies with z
- Origin of z coordinate is at the beam waist
- Rayleigh length z_R defines collimation distance from focal plane

$$z_R = \frac{\pi w_0^2}{\lambda / n} = \frac{\text{beam area}}{\text{wavelength in medium}}$$

b = confocal parameter
= depth of focus

$$w(z) = w_0 \sqrt{1 + \frac{z^2}{z_R^2}}$$



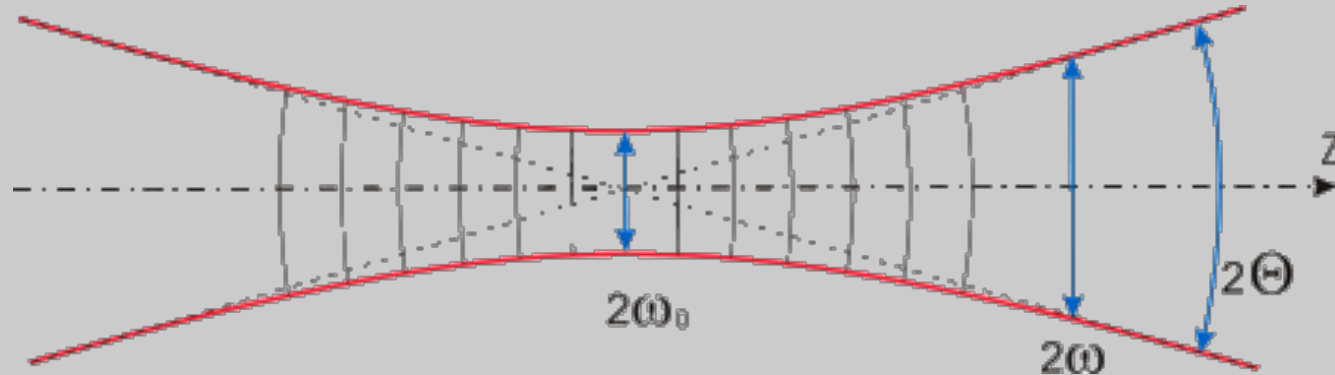
Geometric limit for $z \gg z_R$

$$w(z) = z \frac{w_0}{z_R} = z \tan \Theta$$

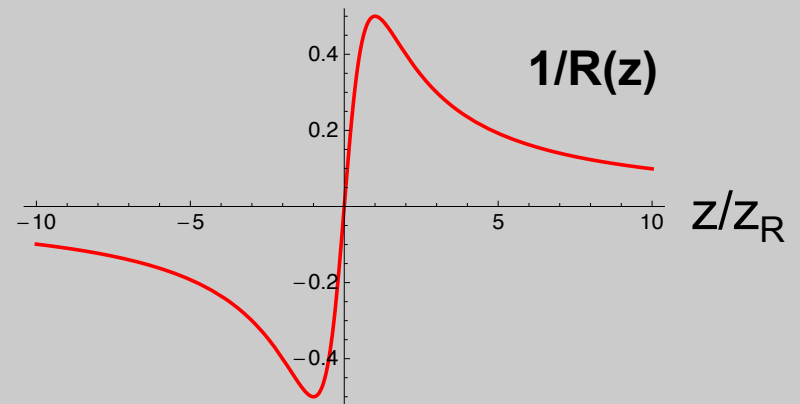
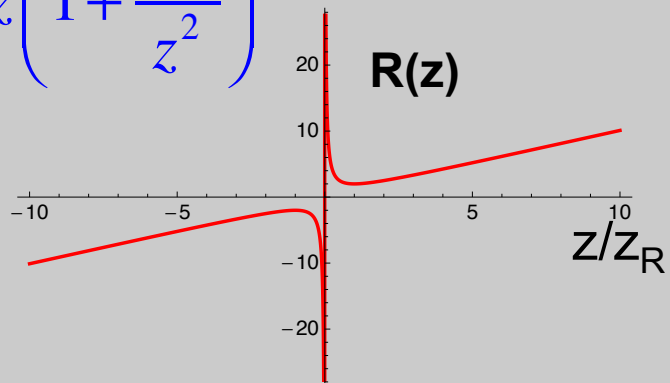
Evolution of wavefronts

$$E(r, z, t) = A_0 e^{-i(kz - \omega t)} \frac{w_0}{w(z)} e^{-\frac{r^2}{w^2(z)}} e^{-i \frac{kr^2}{2R(z)}} e^{i\eta(z)}$$

- Wavefront curvature evolves with z as beam size changes



$$R(z) = z \left(1 + \frac{z_R^2}{z^2} \right)$$



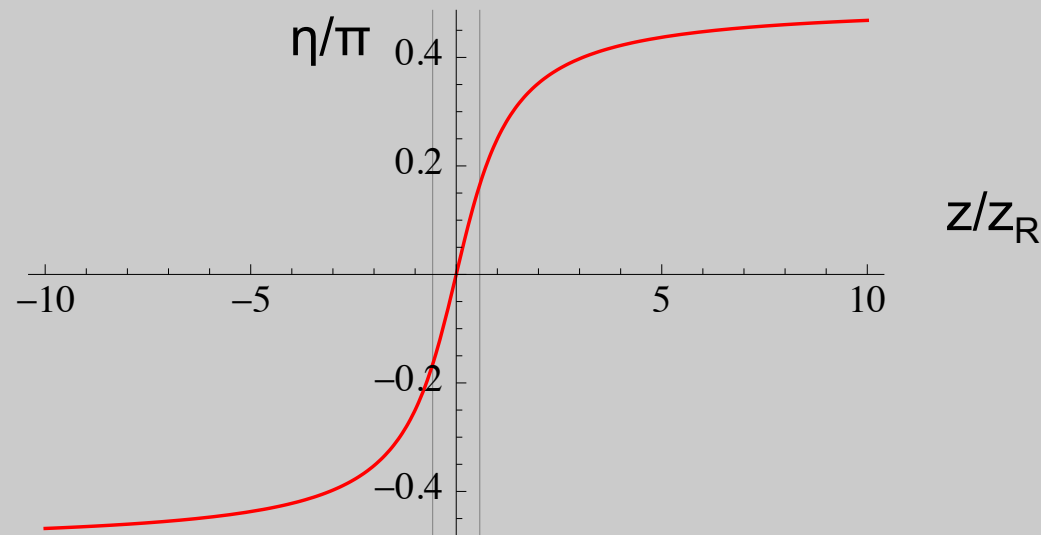
On-axis phase: Gouy phase

$$E(r, z, t) = A_0 e^{-i(kz - \eta(z) - \omega t)} \frac{W_0}{w(z)} e^{-\frac{r^2}{w^2(z)}} e^{-i\frac{kr^2}{2R(z)}}$$

- Because the wavefront changes from focusing to defocusing, on-axis phase advances with z

Gouy phase

$$\eta(z) = \arctan\left(\frac{z}{z_R}\right)$$



Higher-order Hermite-Gauss modes

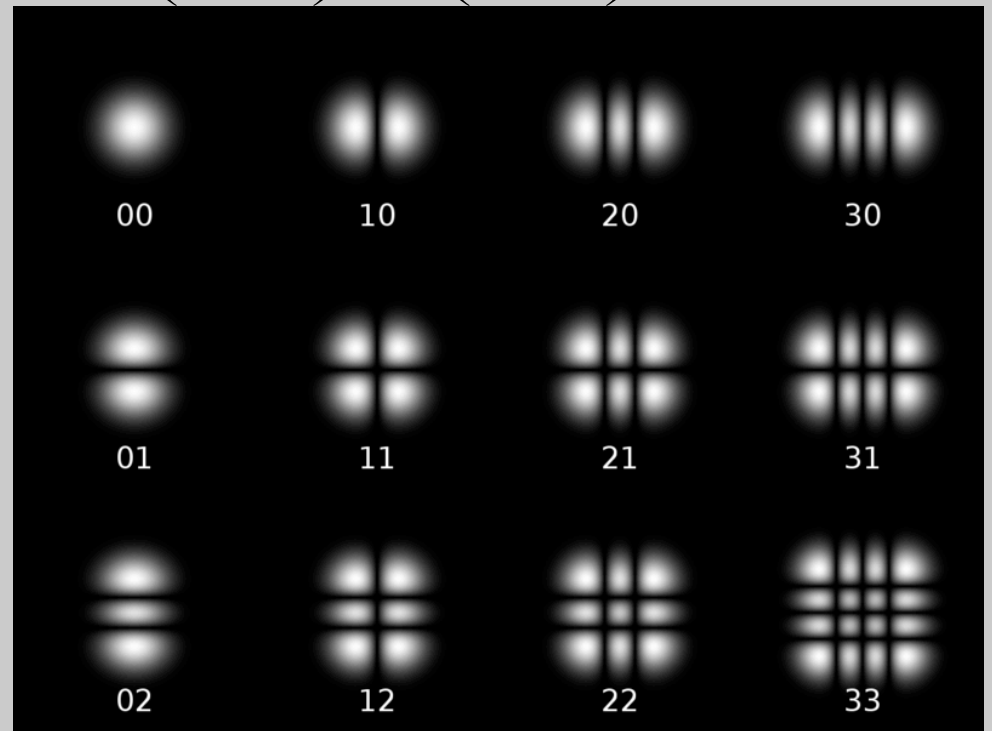
- The Gaussian beam is just the lowest order mode solution to the wave equation
- x, y coordinates: Hermite-Gaussian modes

$$E(x, y, z) = A_0 e^{-i(kz - \eta_{lm}(z))} \frac{w_0}{w(z)} e^{-\frac{x^2 + y^2}{w^2(z)}} H_l \left(\frac{\sqrt{2}x}{w(z)} \right) H_m \left(\frac{\sqrt{2}y}{w(z)} \right) e^{-i\frac{k(x^2 + y^2)}{2R(z)}}$$

$$\eta_{lm} = (l + m + 1) \tan^{-1} \left(\frac{z}{z_R} \right)$$

Transverse profile is maintained during propagation (scaled with $w(z)$)

Hermite-Gauss functions are the same as solutions to quantum SHO

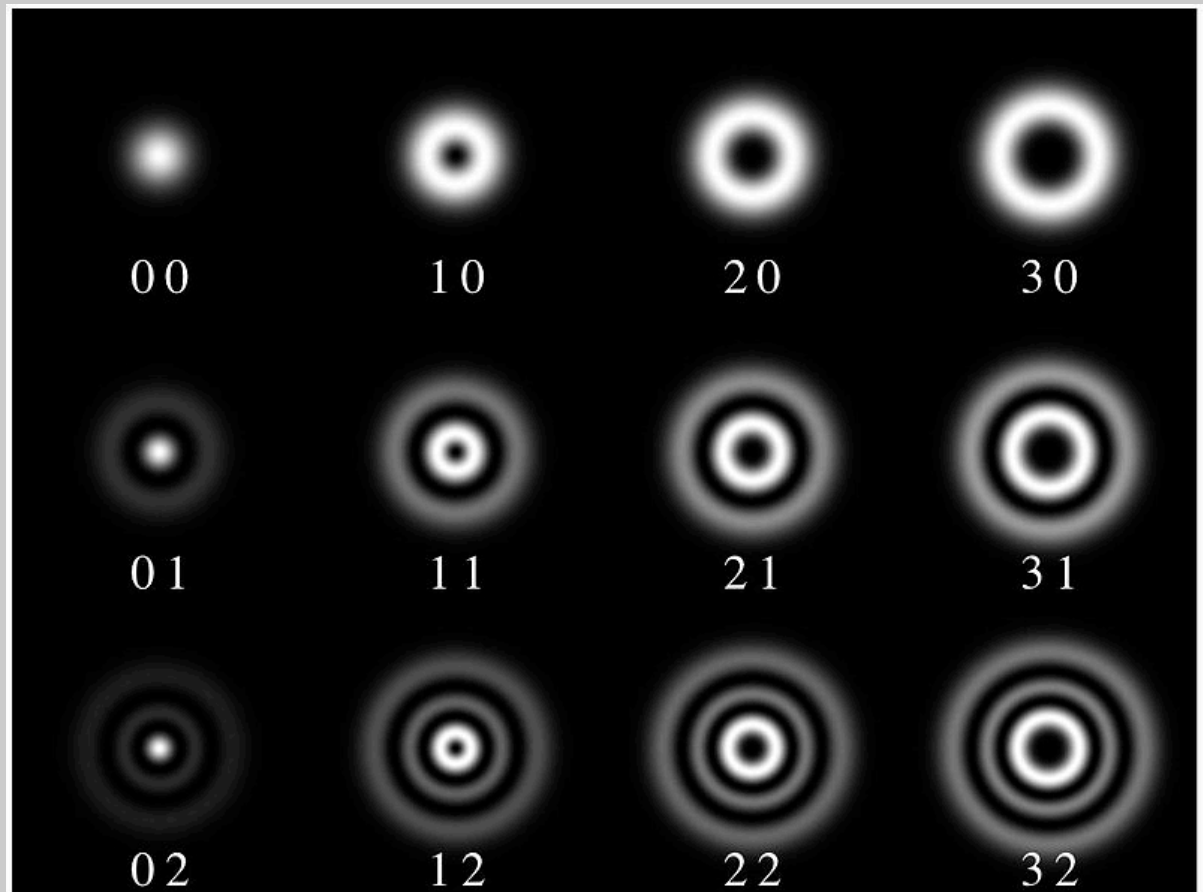


Higher-order LaGuerre-Gauss modes

- In cylindrical coordinates, alternate representation
- Azimuthal phase $\exp[im\phi]$ “vortex” phase

Example:

LG10 mode is a linear combination of HG10 and HG01



Complex q vs standard form

$$u(r, z) = \frac{z_R}{q(z)} e^{-ik \frac{r^2}{2q(z)}} \quad \text{with} \quad \frac{1}{q(z)} = \frac{1}{R(z)} - i \frac{\lambda}{\pi w^2(z)}$$

Expand exponential:

$$\begin{aligned} \exp\left[-ik \frac{r^2}{2q(z)}\right] &= \exp\left[-ik \frac{r^2}{2} \left(\frac{1}{R(z)} - i \frac{\lambda}{\pi w^2(z)}\right)\right] \\ &= \exp\left[-ik \frac{r^2}{2} \frac{1}{R(z)} - i \frac{2\pi r^2}{\lambda} \frac{1}{2} \left(-i \frac{\lambda}{\pi w^2(z)}\right)\right] = e^{-ik \frac{r^2}{2R(z)}} e^{-\frac{r^2}{w^2(z)}} \end{aligned}$$

Expand leading inverse q:

$$a + ib = \sqrt{a^2 + b^2} e^{i \arctan(b/a)}$$

$$\begin{aligned} \frac{1}{q(z)} &= \left(\frac{z}{z^2 + z_R^2} - i \frac{z_R}{z^2 + z_R^2}\right) = -i \left(\frac{z_R + iz}{z^2 + z_R^2}\right) = -i \left(\frac{\sqrt{z^2 + z_R^2}}{z^2 + z_R^2}\right) e^{i \arctan(z/z_R)} \\ &= -i \left(\frac{1}{z_R \sqrt{1 + z^2/z_R^2}}\right) e^{i \arctan(z/z_R)} = \frac{w_0}{i z_R w(z)} e^{i \eta(z)} \end{aligned}$$

Gaussian beams and ABCD

- General expression

$$q_1 = \frac{Aq_0 + B}{Cq_0 + D} \qquad \frac{1}{q(z)} = \frac{1}{R(z)} - i \frac{\lambda}{\pi w^2(z)}$$

- Since q is defined through its inverse, alternate:

$$q_1^{-1} = \frac{C + Dq_0^{-1}}{A + Bq_0^{-1}}$$

- Note that ABCD matrices are the same as for raytrace
- Application is **not** a multiplication like matrix.vector

Simple examples

- translation

$$\frac{1}{q(z)} = \frac{1}{R(z)} - i \frac{\lambda}{\pi w^2(z)} = \frac{1}{z \left(1 + \frac{z_R^2}{z^2}\right)} - i \frac{\lambda}{\pi w_0^2 \left(1 + \frac{z^2}{z_R^2}\right)}$$

$$= \frac{1}{z_R \left(1 + \frac{z^2}{z_R^2}\right)} (z/z_R - i)$$

$$q(z) = z_R \left(1 + \frac{z^2}{z_R^2}\right) \frac{1}{(z/z_R - i)}$$

$$= z_R \left(1 + \frac{z^2}{z_R^2}\right) \frac{z/z_R + i}{\left(1 + \frac{z^2}{z_R^2}\right)} = z + iz_R$$

$$R(z) = z \left(1 + \frac{z_R^2}{z^2}\right)$$

$$w(z) = w_0 \sqrt{1 + \frac{z^2}{z_R^2}}$$

$$q(z) = z + iz_R \rightarrow q_1 = z_0 + L + iz_R$$

ABCD for translation:

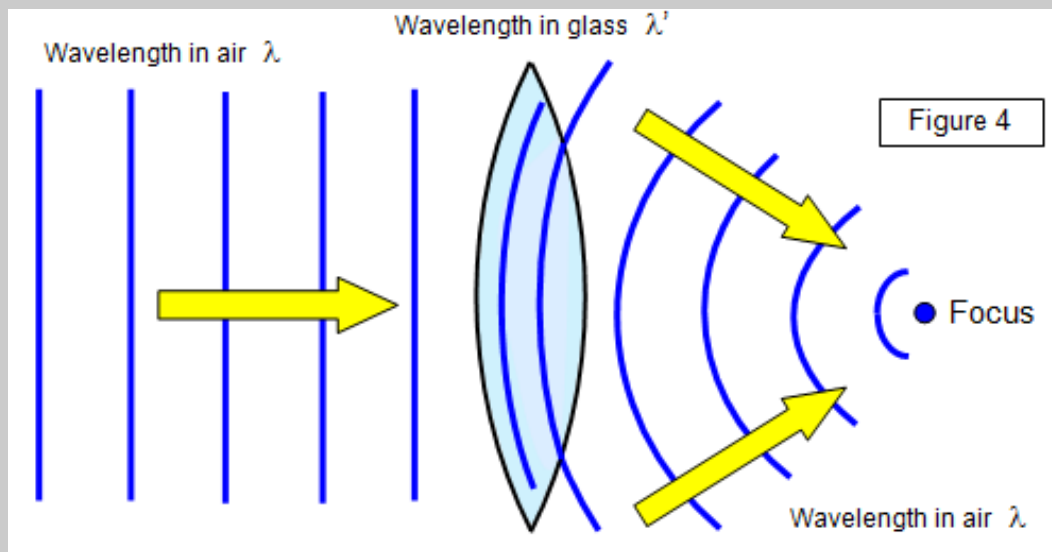
$$\begin{pmatrix} 1 & L \\ 0 & 1 \end{pmatrix}$$

$$q_1 = \frac{Aq_0 + B}{Cq_0 + D} = q_0 + L$$

Simple examples

- Focusing by a lens

- Radius of curvature is modified by lens: $\frac{1}{R'} = \frac{1}{R} - \frac{1}{f}$



Focusing by lens induces a negative ROC

$$\frac{1}{q_1} = \frac{1}{R} - \frac{1}{f} - i \frac{\lambda}{\pi w^2} = \frac{1}{q_0} - \frac{1}{f}$$

$$q_1^{-1} = \frac{C + Dq_0^{-1}}{A + Bq_0^{-1}} \quad \begin{pmatrix} 1 & 0 \\ -1/f & 1 \end{pmatrix}$$

Focusing a Gaussian beam by a lens

- For a beam waist at lens entrance, distance from lens to focused waist is not exactly = f

- Define variables:

w_{01} (w_{02}) = input (focused) beam waist radius

z_{R1} (z_{R2}) = rayleigh range for input (focused) beam

z_m = distance from lens to focused beam waist

- Use Gaussian beam equations to back propagate to lens

$$w_{01} = w(z = -z_m) = w_{02} \sqrt{1 + \frac{z_m^2}{z_{R2}^2}} \quad \rightarrow \quad z_{R1} = \frac{\pi w_{01}^2}{\lambda} = z_{R2} \left(1 + \frac{z_m^2}{z_{R2}^2} \right)$$

$$R(z = -z_m) = -f = -z_m \left(1 + \frac{z_{R2}^2}{z_m^2} \right)$$

- Divide equations:

$$\rightarrow z_{R1} = \frac{\pi w_{01}^2}{\lambda} = z_{R2} \left(1 + \frac{z_m^2}{z_{R2}^2} \right)$$