

## Rectangular metal waveguides

Solve for longitudinal field

TE: solve for  $B_z$  with  $\partial B_z / \partial n = 0$   
i.e. zero slope at walls

TM: solve for  $E_z$  with  $E_z = 0$  at walls.

extend 1-D solutions -

I remember separation of variables  $\rightarrow$  product of sol's

$$\text{TE: } B_z(x, y, z) = B_{z0} \cos\left(\frac{m\pi}{a}x\right) \cos\left(\frac{n\pi}{b}y\right) e^{i(k_z z - \omega t)}$$

modes identified by index

TE<sub>mn</sub>

propagation constant  $k_z^{(m,n)} = k_z$

$$k_z = \sqrt{k_0^2 - k_x^2 - k_y^2} \\ = \left( \frac{\omega^2}{c^2} - \left(\frac{m\pi}{a}\right)^2 - \left(\frac{n\pi}{b}\right)^2 \right)^{1/2}$$

if  $a > b$ , lowest mode (largest  $k_z$ ) is TE<sub>10</sub>

(TE<sub>00</sub> = TEM<sub>00</sub> can't propagate)

$\rightarrow$  cutoff for any mode is where  $k_z = 0$

as freq. is tuned, reach diff't cutoffs;

$$\frac{\omega_{mn}^2}{c^2} = \left(\frac{m\pi}{a}\right)^2 + \left(\frac{n\pi}{b}\right)^2 \rightarrow \omega_{mn} = \pi c \sqrt{\frac{m^2}{a^2} + \frac{n^2}{b^2}}$$

$\rightarrow$  single-mode: if  $\omega_{10} < \omega < \omega_{01}$

this range is single-mode bandwidth

# Dielectric waveguides

qualitative differences

- loss-free guiding by TIR

- evanescent wave exists in cladding

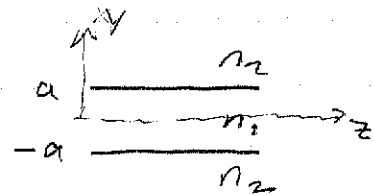
must match functions at boundaries.

- used in IR, visible, UV part of spectrum

- lowest order mode of symmetric vs. is not cut off

- possible to have gradient index

EM solution for modes. one-D slab



$$\nabla_{\perp}^2 \vec{E}_T + \epsilon(y) k_0^2 \vec{E}_T = k_z^2 \vec{E}_T$$

$$\epsilon(x) = n^2(y)$$

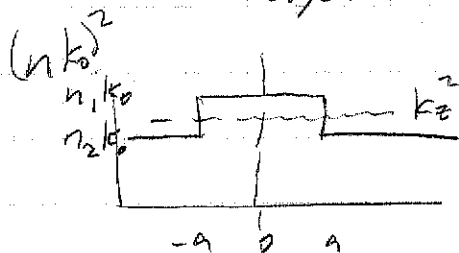
qualitative solutions:

QM equivalent pot'l

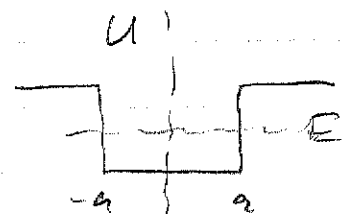
$$U(y) \sim -n^2(y) k_0^2$$

" eigenval

$$E \sim -k_z^2$$



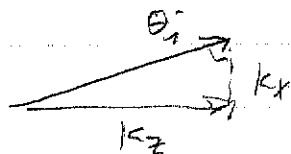
QM



•  $k_z$  is bounded by  $n_2 k_0$  to  $n_1 k_0$  for guided mode.

• lowest modes:  $k_z \lesssim n_1 k_0$   
cutoff  $k_z \approx n_2 k_0$

• use  $\infty$  well type solutions to estimate # modes



$$n_1 \sin \theta_c = n_2$$

$$n_1 k_z / n_1 k_0 = n_2$$

At cutoff (dielectric case)  $k_z = n_2 k_0$   
 in cladding  $k_y = 0$ , evanescent field isn't damped

→ estimate # bound modes using metal w.g. dispersion  
 inside w.g. (metal)

$$k_y = \frac{m\pi}{2a} \rightarrow k_z^2 = n_1^2 k_0^2 - \frac{m^2 \pi^2}{4a^2} \geq n_2^2 k_0^2 \quad \text{at cutoff}$$

solve for  $m$ : bound if inequal. is true.

$$m^2 \leq (n_1^2 - n_2^2) k_0^2 a^2 \frac{4}{\pi^2}$$

$$V\text{-number} \quad V \equiv (n_1^2 - n_2^2)^{1/2} k_0 a$$

mode  $m$  is bound if

$$m < V \cdot 2/\pi \quad (\text{estimate})$$

estimate tends to be low by 1 or 2 modes.

$V \approx \# \text{ bound modes.}$

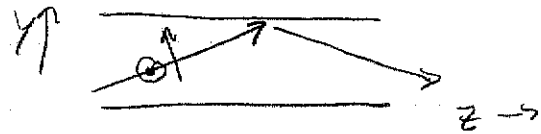
Solve for modes

$$\frac{\partial^2 \vec{E}}{\partial y^2} = - (n_i^2 k_0^2 - k_z^2) \vec{E} \quad i=1,2$$

here, we'll solve for field that is purely transverse

TE: solve for  $E_x$

TM: solve for  $B_x$



most cases,

$$\frac{n_1 - n_2}{n_1} \ll 1 \quad \text{"weak-guiding"}$$

ignore variation in  $\epsilon$  so that  $\nabla \cdot (\epsilon \vec{E}) \approx \epsilon \nabla \cdot \vec{E}$

→ modes are close to TEM

Note  $k_y$ 's depend on region.  $n_1 k_0$

For  $|y| < a$

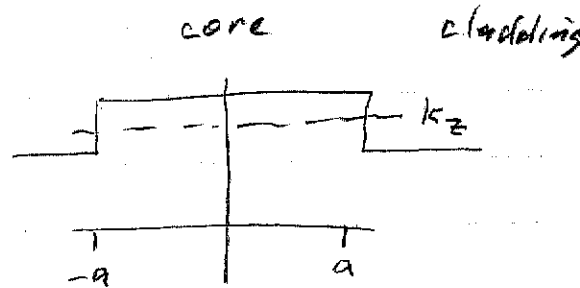
$k_y = \text{real}$ , oscill. solns

let  $k_y = \alpha$  in core

For  $|y| > a$

$k_y = \text{imag}$  (evanescent wave)

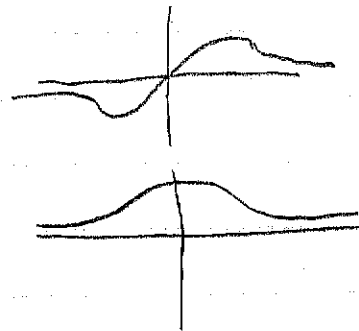
let  $k_y = i\beta$  in cladding.  $E \sim e^{\pm \beta x}$



Take advantage of symmetry:

odd  $\rightarrow \sin \alpha y$

even  $\rightarrow \cos \alpha y$



match at one boundary.

TE even solns

$$E_x = E_1 \cos \alpha y \quad \text{core}$$

$$= E_2 e^{-\beta y} \quad y > a \quad \text{cladding}$$

at  $y=a$  match tang. compon.

$$E_1 \cos \alpha a = E_2 e^{-\beta a}$$

second B.C. from  $\vec{B}$   $\mu=1$  everywhere, all  $\vec{B}$  cont.

$$\nabla \times \vec{E} = i \omega \vec{B}$$

$$\begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \partial_x & \partial_y & \partial_z \\ E_x & 0 & 0 \end{vmatrix} = \hat{y} \partial_z E_x - \hat{z} \partial_y E_x = i \frac{\omega}{c} \vec{B}$$

$$\Delta B_z = 0 \rightarrow \Delta(\partial_y E_x) = 0 \therefore \text{match slope.}$$

$$E_x' \Big|_a = -\alpha E_1 \sin \alpha a \quad \text{core}$$

$$= -\beta E_2 e^{-\beta a} \quad \text{cladding}$$

divide two eqns, eliminate  $E_1, E_2$

$$\alpha a \tan \alpha a = \beta a$$

odd solution  $\rightarrow \alpha a \cot \alpha a = -\beta a$

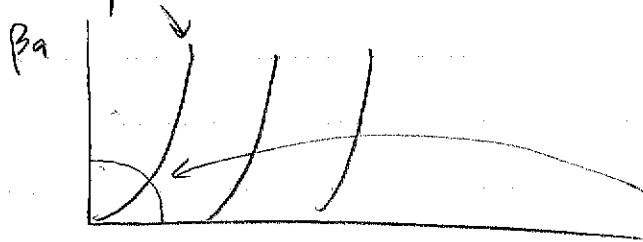
ultimately  $k_z$  is eigenvalue.

$$\alpha^2 = n_1^2 k_0^2 - k_z^2$$

$$\beta^2 = -(n_2^2 k_0^2 - k_z^2)$$

note  $\alpha^2 + \beta^2 = n_1^2 k_0^2 - n_2^2 k_0^2$   
 $= V^2/a^2$

plot  $\beta a$  as fun of  $\alpha a$



also plot  $\beta a = \sqrt{V^2 - (\alpha a)^2}$  circles

intersect  $\rightarrow$  modes.

numerically find roots.