

Reflection from metals

review boundary conditions

$$\nabla \cdot \vec{D} = 4\pi \rho_A \quad \rightarrow \quad \underline{\epsilon_1 E_1^\perp - \epsilon_2 E_2^\perp = 4\pi \rho_{SA}}$$

$$\nabla \cdot \vec{B} = 0 \quad \rightarrow \quad \underline{B_1^\perp - B_2^\perp = 0}$$

free surface charge

$$\nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{B}}{\partial t} \quad \rightarrow \quad \underline{E_1^\parallel - E_2^\parallel = 0}$$

$$\nabla \times \vec{H} = +\frac{1}{c} \frac{\partial \vec{D}}{\partial t} + \frac{4\pi}{c} \vec{J} \quad \rightarrow \quad \underline{H_1^\parallel - H_2^\parallel = \frac{\vec{J}_{SA} \times \hat{n}}{c}}$$

free surface current

but if $\vec{J} = \sigma \vec{E}$

a surface current implies a jump in E^\parallel

$$\vec{J} = \int_{SA} \vec{J}(x, y) \delta(z) dz$$

which violates continuity of E^\parallel



∴ no surface currents.

Also ignore surface charge too as before.

∴ B.C. same as in dielectrics, we can use + extend solutions derived earlier w/ complex index

normal incidence

$$E_1^0 = \frac{\tilde{n}_2 - n_1}{\tilde{n}_2 + n_1} E_0^0 \quad \text{reflection}$$

\tilde{r}

$$E_2^0 = \frac{2n_1}{\tilde{n}_2 + n_1} E_0^0 \quad \text{transmitted}$$

\tilde{t}

note \tilde{r}, \tilde{E} are complex \rightarrow phase shifts.

limit high σ

$$\tilde{r}_2 = \sqrt{E_2 + \frac{i4\pi\sigma_2}{\omega}} \doteq \sqrt{i \frac{4\pi\sigma_2}{\omega}}$$

remember $\delta = \frac{c}{\sqrt{2\pi\sigma\omega}}$ = skin depth. $\sqrt{2\pi\sigma} = \frac{c}{\delta\omega}$

$$\rightarrow \tilde{r}_2 = \frac{(1+i)}{\sqrt{2}} \sqrt{\frac{4\pi\sigma_2}{\omega}} = \frac{(1+i)c}{\delta\omega} = \frac{1+i}{k_{mc}\delta}$$

now calc \tilde{r}

$$\tilde{r} = \frac{1+i - n_1 k_{mc}\delta}{1+i + n_1 k_{mc}\delta}$$

\rightarrow sign change by our def'n

for $\delta \ll \lambda/n_1$, \tilde{r} close to 1 $|1+i|^2 = 2$

$$\tilde{r} \approx \frac{(1+i - \frac{n_1 k_{mc}\delta}{\sqrt{2}})^2}{2} \left. \vphantom{\frac{(1+i - \frac{n_1 k_{mc}\delta}{\sqrt{2}})^2}{2}} \right\} \text{ 9 kiff}$$

$$\approx \frac{1+i}{\sqrt{2}} - \frac{2n_1 k_{mc}\delta}{\sqrt{2}}$$

$$|\tilde{r}|^2 = R \approx \frac{1}{2}(1 - 2n_1 k_{mc}\delta)^2 + \frac{1}{2}$$

$$\approx 1 - 2n_1 k_{mc}\delta \quad \rightarrow \text{quant losses}$$

~~phase $\tan \phi = \frac{\text{Im } \tilde{r}}{\text{Re } \tilde{r}} = \frac{1/\sqrt{2}}{1/2(1 - 2n_1 k_{mc}\delta)}$~~

$$\approx 1 + 2n_1 k_{mc}\delta$$

Oblique incidence onto metal surface.

- continue to use Fresnel equations
- be careful with sign conventions
 - best to just force $r \rightarrow -1$ at $\theta = 0^\circ$ for both r_\perp and r_\parallel
- variable phase shifts with θ , and polarization.
 - reflectivity is always best with "s"

wave inside metal:

use Fresnel eq. to get ampl, phase.

internal wave is then

$$E_0^o \text{ to } e^{-i(k_x x + k_z z - \omega t)}$$

now $k_x x \rightarrow k_{inc} \sin \theta_0 \cdot x$ is still the same. (just as in TIR)

$k_z \rightarrow$ complex (not pure imag)
 $\text{Re}(k_z) \rightarrow$ osc. portion.

\therefore loss is only in z direction.

phase fronts are in direction of $\text{Re}(\vec{k})$:

$$k_x x + \text{Re}(k_z) z$$

in general, this is different than Snell's law

Guided waves.

guiding by metal, TIR, refractive index gradient,
 photonic band gap / Bragg diffraction.

applications

RF: accelerators

microwaves: metal "pipes"

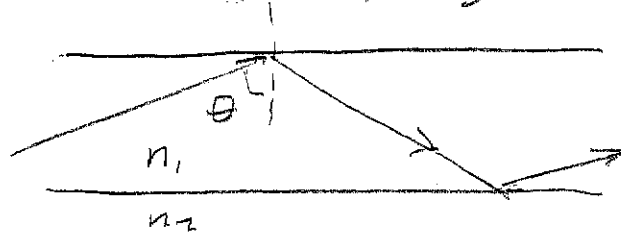
optical: fibers, integrated optics, photonic crystals.

x-ray: capillary tubes.

dynamic mag.: plasma, self-focusing...

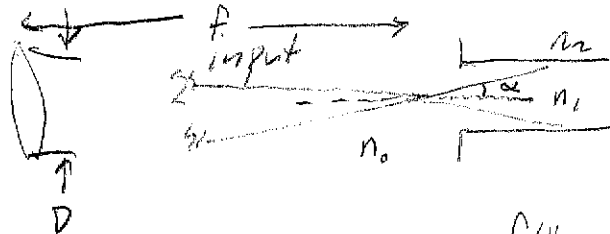
distinguishing features:

$\lambda/a \ll 1 \rightarrow$ "light pipe" guiding, no mode structure



if dielectric $n_1 = \text{core}$ $n_2 = \text{cladding}$

$$\sin \theta_c = n_2/n_1 \quad n_1 > n_2$$



core: $f/\#$ f/D

num. aperture: $NA \equiv n_0 \sin \alpha_{max}$

rays $\rightarrow \vec{k} = \hat{x}k_x + \hat{y}k_y + \hat{z}k_z$

θ will connect to modes

guiding condition \rightarrow # guided modes