Interaction of light with atoms: Line broadening and saturation

Collisional broadening

Doppler broadening

Saturation:

solving CW equilibrium rate equations

saturation with short pulses, saturation fluence

Additional effects found in real systems

- An atom or ion in influenced by the external surroundings in several ways:
 - blackbody EM background: radiatively establishes a thermal (Boltzmann) population distribution
 - Collisions (other atoms or electrons) broaden energy levels (and linewidths) and can also lead to population changes
 - Local fields from a lattice can broaden lines

Types of broadening

- Homogeneous broadening: all individual atoms are broadened by the same amount
- Inhomogeneous broadening: each atom is shifted (e.g. Doppler) so that the ensemble has a broader spectrum



Collisional broadening

- Elastic collisions don't cause transition, but interrupt the phase
- Timescales:
 - Period of EM cycle much less than radiative lifetime
 - Avg time btw collisions < lifetime
 - Duration of a collision << time btw coll, lifetime





 $\Delta \tau_c \ll \tau_c, \tau$

Calculating collisional broadening linewidth

- Calculation:
 - Fourier Transform over time 0 to τ_1 to get lineshape for a specific oscillation length
 - Average over probability of a given time between collisions:

$$P(\tau_1)d\tau_1 = \frac{1}{\tau_c}e^{-\tau_1/\tau_c}d\tau_1$$

Result: Lorentzian shape with new width

 $\Delta v = \gamma / 2\pi + 1 / \pi \tau_c$

 All atoms see the same collision rate, so collisional broadening is homogeneous

Doppler broadening

• From relative velocity of atom to input beam, Doppler shift:

$$V_0' = \frac{V_0}{1 - v_z / c}$$
 Beam propagating in z direction

Each atom in distribution is shifted according to its velocity

Boltzmann distribution

$$P(\mathbf{v}_z) \sim \exp\left[-\frac{1}{2}Mv_z^2 / k_BT\right]$$

• Average over distribution to get effective lineshape:

$$g^{*}(v - v_{0}) = \frac{1}{v_{0}} \left(\frac{Mc^{2}}{2\pi k_{B}T}\right)^{1/2} \exp\left\{\frac{Mc^{2}}{2k_{B}T} \frac{(v - v_{0})^{2}}{v_{0}^{2}}\right\}$$

FWHM: $\Delta v_{0}^{*} = 2v_{0} \left[\frac{2k_{B}T\ln 2}{Mc^{2}}\right]^{1/2}$

Doppler broadening in HeNe lasers

$$\Delta v_0^* = 2v_0 \left[\frac{2k_B T \ln 2}{Mc^2} \right]^{1/2}$$

$$\lambda_0 = 632.8 \text{ nm}$$

$$v_0 = 4.74 \times 10^{14} \text{ s}^{-1}$$

$$M = 20.12 \text{ amu} = 3.34 \times 10^{-26} \text{kg}$$
 For Neon

$$k_B T = 1/40 eV = 4 \times 10^{-21} J$$

$$\Delta v_0^* = 1.55 GHz$$

Inhomogeneous vs homogeneous broadening

- Homogeneous broadening: every atom is broadened by same shape
 - Radiative, collisional, phonon
 - All atoms participate in absorption or gain
- Inhomogeneous broadening:
 - Doppler broadening
 - Absorption or gain only by atoms in resonance
 - Leads to "spectral hole burning"





Population dynamics of absorption

• Closed 2 level system, assume $g_1 = g_2$

$$\begin{bmatrix} \mathbf{W} \, \mathbf{N}_{1} & \mathbf{W} \, \mathbf{N}_{2} & \mathbf{H} \, \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} & \mathbf{V} \, \mathbf{V}_{2} & \mathbf{H} \, \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} & \mathbf{W} \, \mathbf{N}_{2} - \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{N}_{2} - \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{A}_{21} \, \mathbf{N}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{V}_{1} - \mathbf{W} \, \mathbf{V}_{2} - \mathbf{V}_{21} \, \mathbf{V}_{2} \\ \mathbf{W} & \mathbf{W}_{1} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} \\ \mathbf{W} & \mathbf{W}_{1} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} \\ \mathbf{W} & \mathbf{W}_{1} - \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} \\ \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W} \, \mathbf{W}_{2} \\ \mathbf{W} \, \mathbf{W}_{2} - \mathbf{W}$$

• Since system is closed, reduce to one equation for population difference:

$$\Delta N = N_1 - N_2 \qquad \rightarrow \frac{dN_2}{dt} = W \Delta N - A_{21}N_2$$

$$\frac{d}{dt}\Delta N = \frac{dN_1}{dt} - \frac{dN_2}{dt} = -2\frac{dN_2}{dt} = -2(W\Delta N - A_{21}N_2)$$

$$N_t = N_1 + N_2 \qquad N_t = \Delta N + 2N_2 \qquad \rightarrow N_2 = \frac{1}{2}(N_t - \Delta N)$$

$$\frac{d}{dt}\Delta N = -2W\Delta N + A_{21}(N_t - \Delta N) = -\Delta N(A_{21} + 2W) + A_{21}N_t$$

Steady-state (CW) solutions for saturated absorption

 For continuous wave operation – all transients have damped out:

$$\frac{d}{dt}\Delta N = -\Delta N (A_{21} + 2W) + A_{21}N_t$$

$$0 = -\Delta N (A_{21} + 2W) + A_{21}N_t$$

$$\Delta N = \frac{A_{21}N_t}{A_{21} + 2W} \qquad A_{21} = 1/\tau_{21}$$

$$\Delta N = \frac{N_t}{1 + 2W\tau_{21}}$$

Saturation of absorption

- The key parameter in this situation is W T_{21}
 - $W_{21} = \rho_v B_{21}$
 - Low intensity, 2W $T_{21} \ll 1$, $\Delta N \approx N_t$
 - High intensity, 2W τ_{21} >> 1, Δ N ≈ 0. Here N₁ ≈ N₂
- Energy balance:

Input power (into 4π) Absorbed by atoms

Stimulated emission (back into beam)

• Radiated power per unit volume:

$$\frac{dP}{dV} = hV_{21}W\Delta N(W) = hV_{21}\frac{N_tW}{1+2W\tau_{21}} \to hV_{21}\frac{N_t}{2\tau_{21}} \quad \text{For W } \tau_{21} >> 1$$

Power radiated in high intensity limit: half of atoms are radiating

$$\Delta N = \frac{N_t}{1 + 2W\tau_{21}}$$

$$\Delta N = N_1 - N_2$$

Saturation intensity

- Absorbed power per atom: $\sigma_{12}I$
- Absorption rate: Absorption rate: $W = \frac{1}{hv_{21}}$ • In steady state: $\frac{\Delta N}{N_t} = \frac{1}{1+2W\tau_{21}} = \frac{1}{1+2\frac{\sigma_{12}I}{hv_{21}}\tau_{21}} = \frac{1}{1+2\frac{\sigma_{12}I}{hv_{21}}\tau_{21}}$
- Saturation intensity for absorption:
 - 2: transition affects both levels at once I_{sat}
 - At I = I_{sat} , stimulated and spontaneous emission rates are equal.
- Intensity-dependent absorption coefficient:

$$\alpha(I) = \frac{\alpha_0}{1 + I/I_{sat}}$$

At high intensity, material absorbs less.

Saturable absorbers are used for pulsed lasers: Q-switching and mode-locking

Saturated CW propagation through absorbing medium

 For a given thickness for an absorbing medium, the transmission will increase with intensity



Dynamic saturation: pulsed input

• Rewrite equation using intensity:

$$\frac{d}{dt}\Delta N = -\Delta N \left(A_{21} + \frac{2\sigma}{hv_{21}} I(t) \right) + A_{21}N_t \equiv -\Delta N \left(A_{21} + \frac{I(t)}{\Gamma_{sat}} \right) + A_{21}N_t$$

Define Γ_{sat} = saturation fluence

- Scaling of equation: determine relative importance of terms
 - Input intensity can be rewritten as:

$$I_{in} = \frac{\Gamma_{in}}{\tau_p}$$

 $\Delta N = N_1 - N_2$

- Rewrite equation:

$$\frac{d}{dt}\Delta N = -\Delta N \left(\frac{1}{\tau_{21}} + \frac{\Gamma_{in}}{\Gamma_{sat}}\frac{1}{\tau_p}\right) + \frac{1}{\tau_{21}}N_t = \frac{2N_2}{\tau_{21}} - \frac{\Gamma_{in}}{\Gamma_{sat}}\frac{1}{\tau_p}\Delta N$$

- Note there are two timescales: T_p and T_{21}
- The weighting of the two controls which we might ignore.

Saturation with short pulse input

$$\frac{d}{dt}\Delta N = 2N_2 \frac{1}{\tau_{21}} - \frac{\Gamma_{in}}{\Gamma_{sat}}\Delta N \frac{1}{\tau_p}$$

• For short pulse input: ignore stimulated emission and fluorescence

$$\frac{\Gamma_{in}}{\Gamma_{sat}} \frac{1}{\tau_p} |\Delta N| \gg \frac{2N_2}{\tau_{21}} \qquad \rightarrow \frac{d}{dt} \Delta N \approx -\frac{\Gamma_{in}}{\Gamma_{sat}} \frac{1}{\tau_p} \Delta N$$
- Put back in terms of time-dependent intensity: $\frac{1}{\Delta N} \frac{d}{dt} \Delta N \approx -\frac{1}{\Gamma_{sat}} T(t)$
- Solve equation by integrating $\rightarrow \ln \left[\frac{\Delta N(t)}{\Delta N(0)}\right] \approx -\frac{1}{\Gamma_{sat}} \int_{0}^{t} I(t') dt'$
- If all in ground state initially, $\Delta N(0) = N_t$

- At end of pulse:
$$\int_{0}^{\infty} I(t')dt' = \Gamma_{in} \longrightarrow \Delta N(\infty) = N_t \exp\left[-\frac{\Gamma_{in}}{\Gamma_{sat}}\right]$$

Short pulse limit

- For short pulse input: $T_p << T_{21}$, so ignore fluorescence
 - Medium just integrates energy of pulse.
 - Example: Ti:sapphire: τ₂₁=3.2µs, τ_p=10ns or 200ns for Q-switched Nd:YAG lasers pumped with flashlamps or CW arc lamps
- Square input pulse
 Ga
 - Gaussian input pulse

$$- \tau = 3$$
, $I_{0/}I_{sat} = 0.1$, (no fluorescence)



Shape of transmitted pulse is affected

Long pulse limit

 For *long* pulse input: τ_p>>τ₂₁, and peak I << I_{sat}, ΔN(t) follows I(t)

 $\rightarrow \frac{d}{dt} \Delta N \ll A_{21} N_t$ $\frac{\Delta N}{N_t} = \frac{1}{1 + I(t)/I_{sat}}$

Quasi-static, quasi-CW limit N_t adiabatically follows I(t)



Gain saturation

• Consider a 4-level system:



No factor of 2 $I_{sat} = \frac{hv_{21}}{\sigma_{21}\tau_{21}} = \frac{\Gamma_{sat}}{\tau_{21}}$ $g(I) = \frac{g_0}{1 + I/I}$

Beam growth during amplification

Calculation just as with absorption

$$\int_{I_0}^{I} \left(\frac{1}{I} + \frac{1}{I_{sat}}\right) dI = + \int_{0}^{L} g_0 \, dz \rightarrow \ln\left[\frac{I(z)}{I(0)}\right] + \frac{I(z) - I(0)}{I_{sat}} = + g_0 z$$
Net gain over 1 absorption length
$$\int_{I_0}^{I_0} \frac{1}{I_{sat}} = 0.1$$

$$\int_{I_0}^{I_0} \frac{1}{I_{sat}} = 0.1$$

$$\int_{I_0}^{I_0} \frac{1}{I_{sat}} = 10$$

Even though saturated gain is low, it is efficient at extracting stored energy

Spatial dependence

- Gain follows distribution of pump intensity
- Spatial variation of gain affects beam profile
- Examples:
 - Iongitudinal pumping with Gaussian beam leads to gain narrowing of spatial profile. More gain in center, less at edges
 - Saturated absorption by a Gaussian beam: saturation in center suppresses intensity there. Leads to widening of output beam.

Pulse amplification: saturated gain algorithm



Example: Ti:sapphire multipass amp

- Seed pulse from pulsed laser oscillator: 1nJ (800nm)
- Amplify to 1mJ, use 7mJ of pump energy (532nm)
- Multipass designs: spatially separate beams

Three-mirror ring preamp:

- Up to 12 passes
- Focused beam in crystal
- 2 mirror alignment

Q-switched Nd;YLF IOW max IOW max III (Sapphire Pulses input)

Bowtie power amp:

- Collimated beam
- 8 mirrors



Multipass design

- Assume uniform pumping with round beams
- Calculate stored fluence and small signal gain
- Use saturated gain expression to calculate new energy after 1st pass
- Subtract extracted energy from stored energy (over seed spot area)
- Repeat for N passes

Conditions: 1nJ seed, 7mJ pump energy, 95% absorption, 10% loss/pass Stored energy: hV_{mad}

$$E_{stor} = E_{pump} \eta_{abs} \frac{h v_{seed}}{h v_{pump}} = 4.4 \, mJ$$

Small signal gain estimate:

$$G_0 = \left(\frac{E_{\text{target}}}{E_{\text{seed}}}\right)^{1/N} \frac{1}{1-L} = 4.42$$

Estimated spot size:

$$A_{pump} = \frac{E_{stor}}{\Gamma_{sat} \ln[G_0]}, \quad w_p = 300 \,\mu m$$

Multipass: Simple calculated results

 Small signal gain estimate works as long as stored energy is not depleted



- Smaller seed size to ensure full overlap with pump
- Avoid damage thresholds for pump and seed
- Saturate at desired energy to reduce noise
- Account for size change in Brewster cut crystal



Polarization issues in pumping birefringent materials

- For Ti:sapphire, both polarizations contribute to seed gain along c-axis
- Much higher pump absorption for E along c-axis

 $- \alpha$ across c-axis is about 40% lower than along c-axis



Transverse Pumping Gain Estimates

- Seed: 2nJ
 - Cavity Losses: ~1%
 - т_{pass}: 1ns
- Pump (CW): 1kW (Total: 2X .5kW Bars)
 - η_{Abs}=63.2%
 - η_{QD}=55.6%
 - $-\eta_{Pump} = \eta_{Abs} \eta_{QD} = 35.1\%$
 - − Heat: ~560 W
 - Significant (Cylindrical) Thermal Lens Expected
 - w=30um
- Single Pass Gain (small signal)
 - Astigmatic Seed: g≈1.64
 - w_x=200um, w_y=30µm
 - Spatially Chirped Seed: g≈1.64
 - w_x=2mm, w_y=30µm

•Multi-Pass Extraction: 37 Passes

-Astigmatic Mode: ~136uJ (small extraction area) -Spatially Chirped:~.53mJ (46% extraction)

Central dip in gain: spatial gain mode *expansion*. This could be used to counter gain narrowing for spatially-chirped seed



Frequency dependence: account for lineshapes

• Absorption and gain coefficients and saturation intensity both depends on frequency

$$\alpha(I,v) = \frac{\alpha_0(v-v_0)}{1+\frac{I(v)}{I_{sat}(v-v_0)}}$$

- For broadband input, saturation changes shape of transmitted spectrum
 - Absorption: power broadening
 - Gain: spectral gain narrowing

Amplified Spontaneous Emission (ASE)

- Spontaneous emission is emitted into 4π steradians, but is amplified on the way out if there is gain.
 - D ______ >
 - ASE can be considered to be a noise source
 - ASE is more directional than fluorescence, but not as directional as a coherent laser beam
 - Some high-gain lasers are essentially ASE sources (no mirrors)
- Implications for amplifier design
 - ASE can deplete stored energy before pulse extraction
 - Use timing and good seed energy to extract energy from medium before ASE
 - Ensure that transverse gain is smaller than longitudinal to avoid parasitic depletion.

Self-absorption and "optically-thick" media

- A related phenomenon for an absorbing medium is when radiation is *absorbed* along the way out.
- More absorption near the line center, so the transmitted light is broader in spectrum.
- For an extended luminous body (e.g. the Sun), the individual spectral lines get merged together to look like the blackbody.