

Anisotropic media: birefringence.

in an isotropic medium:

$$\vec{D} = \epsilon \vec{E}$$

$$\vec{D} = \epsilon_0 \epsilon \vec{E}$$

if linear,  $\epsilon$  doesn't depend on  $\vec{E}$   
 $\vec{D} \parallel \vec{E}$

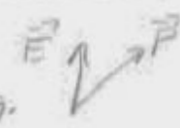
in an anisotropic medium,  $\vec{D} \not\parallel \vec{E}$

$$\vec{D} = \vec{E} + 4\pi \vec{P}$$

$$\vec{D} = \epsilon_0 \vec{E} + \vec{P}$$

↑  
applied

↑  
induced polarization

due to asymmetry of crystal,  $\vec{P} \not\parallel \vec{E}$  e.g. 

write  $\vec{D} = \vec{\epsilon} \cdot \vec{E}$

$\vec{\epsilon}$  = dielectric tensor =

$$\begin{pmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{21} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{31} & \epsilon_{32} & \epsilon_{33} \end{pmatrix}$$

Guenther p. 35

if material is not lossy,  
energy considerations  $\rightarrow$

$\vec{\epsilon}$  is Hermitian  $\epsilon_{ij} = \epsilon_{ji}$

We can choose the orientation of coordinates to diagonalize

$$\rightarrow \begin{pmatrix} D_x \\ D_y \\ D_z \end{pmatrix} = \begin{pmatrix} \epsilon_x & & \\ & \epsilon_y & \\ & & \epsilon_z \end{pmatrix} \begin{pmatrix} E_x \\ E_y \\ E_z \end{pmatrix}$$

(in most crystals)

this coord. system is aligned along the crystal axes.

so if  $\vec{E} = E_x \hat{x}$ ,

$$\vec{D} = D_x \hat{x} = \epsilon_x E_x \text{ only.}$$

biaxial crystal:  $\epsilon_x \neq \epsilon_y \neq \epsilon_z$

uniaxial crystal: one pair is the same. e.g.  $\epsilon_x = \epsilon_y \neq \epsilon_z$

isotropic crystal:  $\epsilon_x = \epsilon_y = \epsilon_z = \epsilon$

$$\vec{D} = \epsilon \begin{pmatrix} 1 & & \\ & 1 & \\ & & 1 \end{pmatrix} \vec{E}$$

"dichroic" absorption depends on polarization e.g. polaroid.

## Wave propagation in birefringent media.

main points:

- 1) if wave propagates so that  $\vec{k}$  is along one of the 3 crystal axes, it propagates normally, with a refractive index assoc. with that crystal axis
- 2) for arbitrary directions of  $\vec{k}$  and  $\vec{E}$  (relative to crystal axes)
 
$$\vec{D} \parallel \vec{E} \quad \text{and} \quad \vec{k} \parallel \vec{S}$$

$$\vec{H} \perp \vec{D}, \vec{E}, \vec{k}, \vec{S}$$
- 3) the index of refraction varies as an ellipse in between the extreme values of  $n$  along the axes.

Vector directions: get these from Maxwell  $(\vec{k} \cdot \vec{r} = \omega t)$   
 for a plane wave: all terms  $(D, E, B, H) \propto e^{i(\vec{k} \cdot \vec{r} - \omega t)}$   
 $\frac{\partial}{\partial t} \rightarrow -i\omega \quad \nabla \cdot \rightarrow i\vec{k} \cdot$

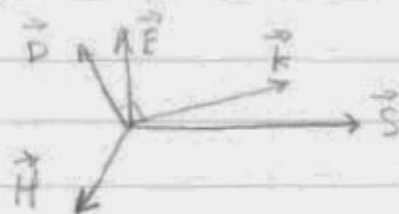
$$\nabla \cdot \vec{D} = 0 \rightarrow \vec{k} \cdot \vec{D} = 0 \quad \therefore \vec{k} \perp \vec{D}$$

$$\nabla \cdot \vec{H} = 0 \rightarrow \vec{k} \cdot \vec{H} = 0 \quad \vec{k} \perp \vec{H} \quad \text{assume non-magnetic}$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \rightarrow \vec{k} \times \vec{E} = \omega \vec{B} \quad \therefore \vec{B} \perp \vec{k}, \vec{E}$$

$$\nabla \times \vec{H} = \frac{\partial \vec{D}}{\partial t} \rightarrow \vec{k} \times \vec{H} = -\omega \vec{D} \quad \therefore \vec{D} \perp \vec{k}, \vec{H}$$

finally  $\vec{S} = \vec{E} \times \vec{H}$  Poynting vector gives direction of energy flow  
 wavefronts are  $\perp \vec{k}$   $\vec{D} \parallel \vec{E}$   
 $\vec{k} \parallel \vec{S}$   
 $\vec{H} \perp \vec{D}, \vec{E}, \vec{k}, \vec{S}$   
 = beam direction



## Index ellipsoid

- allows calculation of  $n(\theta, \phi)$
- important for tuning phase matching.

energy density is a scalar:

$$2U_E = \vec{D} \cdot \vec{E} \quad \text{this connects the vector components}$$

$$D_x = \epsilon_x E_x, \quad D_y = \epsilon_y E_y, \quad D_z = \epsilon_z E_z$$

in crystal coord. system.  $\epsilon_x = \epsilon_0 n_x^2$ , etc

$$\therefore 2U_E = \frac{D_x^2}{\epsilon_x} + \frac{D_y^2}{\epsilon_y} + \frac{D_z^2}{\epsilon_z}$$

put into a form like an ellipsoid:

$$\frac{1}{2U_E \epsilon_0} \left( \frac{D_x^2}{n_x^2} + \frac{D_y^2}{n_y^2} + \frac{D_z^2}{n_z^2} \right) = 1$$

define a unit vector  $\hat{d} = \vec{D} / 2U_E \epsilon_0 \rightarrow$  points along  $\vec{D}$

$$\frac{\hat{d}_x^2}{n_x^2} + \frac{\hat{d}_y^2}{n_y^2} + \frac{\hat{d}_z^2}{n_z^2} = 1 \quad \text{eqn. of ellipse}$$

For phase matching, we need to know  $\vec{k}$  inside crystal

$\rightarrow$  phase, group velocity

let  $\hat{k} = \vec{k} / k_0$  normalized to vacuum  $k_0 = \omega / c$

suppose  $\vec{k}, \vec{D}$  are in x-z plane of crystal  $\vec{k} \perp \vec{D}$

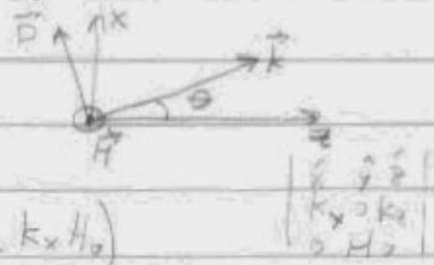
$\rightarrow$  in a uniaxial crystal,  $n_z = n_o$   $n_x = n_e$

$$\vec{k} = \hat{x} k \sin \theta + \hat{z} k \cos \theta$$

refractive index will be between  $n_e, n_o$

write  $k = n_o(\theta) k_0$  find  $n_o(\theta)$

$$\vec{D} = -\frac{1}{\omega} \vec{k} \times \vec{H} = -\frac{1}{\omega} \left( \hat{x} k_z H_0 + \hat{z} k_x H_0 \right)$$



$$D_x = \frac{k_z}{\omega} H_0 = H_0 \frac{n}{c} \cos \theta \quad D_z = -\frac{k_x}{\omega} H_0 = -H_0 \frac{n}{c} \sin \theta$$

Put these  $\vec{D}$  components into ellipsoid eqn.

$$\frac{1}{2U_e \epsilon_0} \frac{n_0^2}{c^2} n^2 \left( \frac{\cos^2 \theta}{n_o^2} + \frac{\sin^2 \theta}{n_e^2} \right) = 1$$

now magnetic energy is  $U_H = \frac{1}{2} \vec{H} \cdot \vec{B} = \frac{1}{2\mu_0} H_0^2$

So now the multiplier in front is

$$\frac{U_H}{U_e} \frac{1}{\epsilon_0 \mu_0 c^2} = \frac{U_H}{U_e} = 1$$

equivalence of  $U_e = U_H$  is shown on next page.

Finally:

$$\frac{1}{n_e^2(\theta)} = \frac{\sin^2 \theta}{n_o^2} + \frac{\cos^2 \theta}{n_e^2}$$

Example: uniaxial crystal

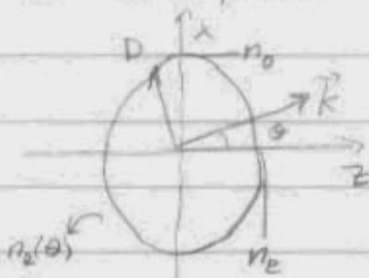
1)  $\vec{E}$  along  $\hat{z}$ : both polarizations  $\rightarrow n = n_o$

2) tilt crystal  $\theta$  away from  $\hat{z}$  in X-Z plane.

$D_y$  still sees  $n_o$

$D_x \rightarrow n_e(\theta)$  given above

where  $\vec{D}$  intersects index ellipsoid  $\rightarrow n_e(\theta)$



Show that  $U_H = U_E$  in an anisotropic medium

(Gaussian units)

energy density in magnetic field:

$$8\pi U_H = \vec{H} \cdot \vec{B}$$

put these in terms of  $\vec{E}$  field

$$\vec{K} \times \vec{E} = \frac{\omega}{c} \mu \vec{H} = \frac{\omega}{c} \vec{B}$$

lets write  $\vec{K}/(\omega/c) = n \vec{k}$

$$\text{so } \vec{H} \cdot \vec{B} = \frac{c}{\mu} (\vec{K} \times \vec{E}) \cdot n (\vec{K} \times \vec{E})$$

$$\text{vector ID } (\vec{a} \times \vec{b}) \cdot (\vec{c} \times \vec{d}) = (\vec{a} \cdot \vec{c})(\vec{b} \cdot \vec{d}) - (\vec{a} \cdot \vec{d})(\vec{b} \cdot \vec{c})$$

(see Jackson inside cover)

$$\vec{H} \cdot \vec{B} = \frac{n^2}{\mu} (E^2 - (\vec{K} \cdot \vec{E})^2)$$

$$\text{Now look at } \vec{E} \cdot \vec{D} = 8\pi U_E$$

represent  $\vec{D}$  in terms of  $\vec{E}$

$$n(\vec{K} \times \vec{E}) = \mu \vec{H}$$

$$n \vec{K} \times (\vec{K} \times \vec{E}) = \mu \vec{K} \times \vec{H} = \frac{1}{\mu} (-\vec{D})$$

$$\text{so } n(\vec{K}(\vec{K} \cdot \vec{E}) - \vec{E}) = -\frac{1}{\mu} \vec{D}$$

$$\therefore \vec{E} \cdot \vec{D} = \frac{n^2}{\mu} (E^2 - (\vec{K} \cdot \vec{E})^2)$$

$$\therefore \vec{E} \cdot \vec{D} = \vec{H} \cdot \vec{B} \text{ and } U_E = U_H$$

## Birefringent phase matching

It is clear from the solutions of the coupled wave eqns. that high efficiency requires

$$\Delta k = k_1 + k_2 - k_3 = 0$$

When  $\Delta k \neq 0$  the yield varies as

$$\sin^2(\Delta k L / 2)$$

$\Delta k = 0$  sets a condition on the refr. index:

$$\Delta k = k_1 + k_2 - k_3 = n_1 \omega_1 + n_2 \omega_2 - n_3 \omega_3$$

as shown in part (2.7.7) this cannot take place with "normal" dispersion, where:  $n_3 > n_1, n_2$

techniques:

- anomalous dispersion: typ  $\omega_3$  on high side of resonance.



example: mixing in gas (VUV)

HTIG

- birefringent PM



neg. v. maximal

> angle-tune

> temperature tune

- Quasi phase matching = periodic modulation at  $\Delta k \neq 0$   
→ slow buildup in signal

## Refraction into birefringent materials (Gветтер appx 13C)

since  $E_{\parallel}$  is conserved across boundary

$$(\vec{E}_1)_{\parallel} e^{i(\vec{k}_1 \cdot \vec{r} - \omega t)} = (\vec{E}_2)_{\parallel} e^{i(\vec{k}_2 \cdot \vec{r} - \omega t)}$$

where  $\vec{r}$  is in x-y plane (on surface)

$$\therefore \text{as usual } \vec{k}_1 \cdot \vec{r} = \vec{k}_2 \cdot \vec{r}$$

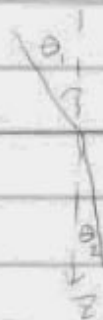
$$k_0 n_1 \sin \theta_1 = k_0 n_2 \sin \theta_2$$

for  $n_2 = n_0$  this is normal Snell's law

for  $n_2 = n_0(\theta_2)$ ,

$\rightarrow$  more complicated relationship

$$\text{use } n_0(\theta) = \left( \frac{\sin^2 \theta_2 + \cos^2 \theta_2}{n_0^2} \right)^{1/2}$$



Birefringent case: most common by far.

2 options -  $\omega_2$  is along lowest index direction.

Type I:

$\omega_1$  and  $\omega_2$  share same polarization.

$$\vec{E}_1 \parallel \vec{E}_2$$

Type II:

$$\vec{E}_1 \perp \vec{E}_2$$

"Type III" also called 90° phase matching.

- like Type I, but input at  $\theta = 90^\circ$  and temperature tuned.

- LiNbO<sub>3</sub> most common.

Angle tuning:

use  $n_e(\theta)$  function

$$\frac{1}{n_e(\theta)^2} = \frac{\sin^2 \theta}{n_e^2} + \frac{\cos^2 \theta}{n_o^2}$$

Ex Type I: neg. uniaxial ( $n_e < n_o$ ) doubling  $\Delta k = 2k_1 - k_2 \Rightarrow \frac{2\omega_1(n_1 - n_2)}{c}$

$$n_e(2\omega, \theta) = n_o(\omega)$$

input  $\vec{E}_1$  along  $n_o$ , vary crystal angle around

$\vec{E}_1$  to tune index of  $\omega_2$

$$\vec{E}_2 \perp \vec{E}_1$$



practical concerns:

- cut crystal for the process
- x-ray diff to get angle close
- protective A/R coating or in cell to keep off water.



• wavelength separations:

- prisms: no background, - polarized (too expensive)

- dichroic mirrors: typ. refl. harmonics at "S"  
transm. fundam. at "P"



for best efficiency

often need multiple mirrors to get rid of fundam.

• temperature stabilization:

- heating to drive off moisture.

- harmonic is often partly absorbed in crystal

$$\rightarrow \Delta T \rightarrow \Delta k$$

$\therefore$  stabilize at  $T \rightarrow T_{room}$ ,

- can fracture  $\Delta k$  with  $\Delta T$

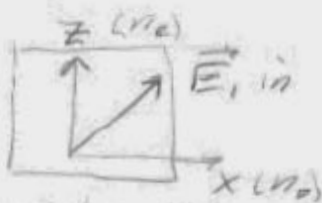
Type II: doubling  $\Delta k = \frac{1}{2}(\omega_1 n_e(\theta, \omega_1) + \omega_1 n_o(\omega_1) - \omega_2 n_e(\theta, \omega_2))$

- often seen with KTP higher nonlinearity.

- tripling after type I doubling.

- equal  $\vec{E}_1$  along  $n_e, n_o$ .

input  
 $\vec{k} \otimes$



output



$\therefore$  output at 45° to input

mirrors out of plane used to flip polarization (typically)