

## Chapter 8

heat and work ~~in a reservoir:  $T = \text{const}$~~  regardless of addition or extraction of heat

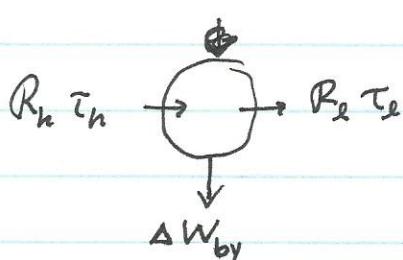
$$\underline{1^{\text{st Law}}} \quad \tilde{Q} = dU - \tilde{W} \quad (= dU + pdV_{\text{gas}}) = Td\sigma$$

$$\therefore \tilde{Q} = Td\sigma$$

$$\Delta Q = \int \tilde{Q} \quad \Delta W_{\text{on}} = \int \tilde{W} \quad \Delta U = \int dU$$

$$\boxed{\Delta U = 0 \Rightarrow \Delta Q_{\text{abs}} = -\Delta W_{\text{on}}} \quad (\text{cycle: } \oint dU = 0 \text{ always})$$

heat  $\rightarrow$  work (engines)



$$\underline{1^{\text{st Law}}} \quad \Delta Q_{\text{abs}} = -\Delta W_{\text{on}} = +\Delta W_{\text{by}} \quad (\Delta U = 0)$$

$$Q_h + Q_e \xrightarrow{\text{heat in}} \cancel{T_h T_e} \xrightarrow{\text{heat out}} Q_e \quad \Delta Q_{\text{abs}} = Q_h - Q_e$$

$$\Delta W_{\text{by}} = Q_h - Q_e = T_h \bar{T}_h - T_e \bar{T}_e$$

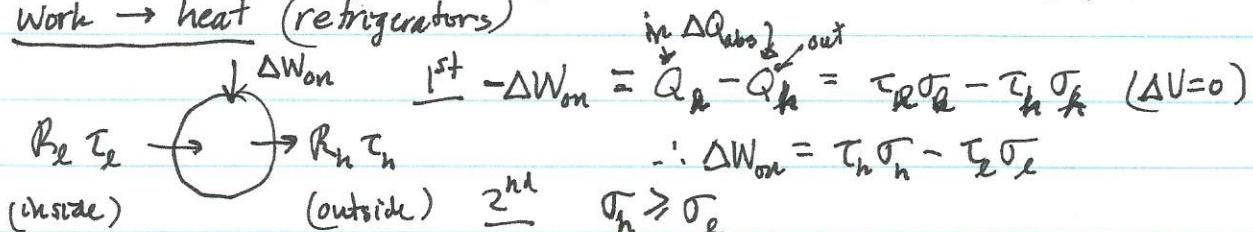
$$\underline{2^{\text{nd Law}}} \quad T_e \geq \bar{T}_h \quad (\text{can't destroy entropy})$$

$$\Delta W_{\text{by}} \leq (T_h - T_e) \bar{T}_h = \left( \frac{T_h - T_e}{T_h} \right) Q_h \equiv \eta_c Q_h$$

$$\left( \frac{\text{Work out}}{\text{heat in}} \right) = \left( \frac{\Delta W_{\text{by}}}{Q_h} \right) \leq \eta_c < 1 \quad \eta \leq \eta_c$$

$\eta_c = 1$  only for  $T_e = 0$  which  
is (3rd Law) unattainable (like  
speed of light)

work  $\rightarrow$  heat (refrigerators)



$$\underline{1^{\text{st}}} \quad -\Delta W_{\text{on}} = \tilde{Q}_h - \tilde{Q}_{\text{out}} = T_h \bar{T}_h - T_e \bar{T}_e \quad (\Delta U = 0)$$

$$\therefore \Delta W_{\text{on}} = T_h \bar{T}_h - T_e \bar{T}_e$$

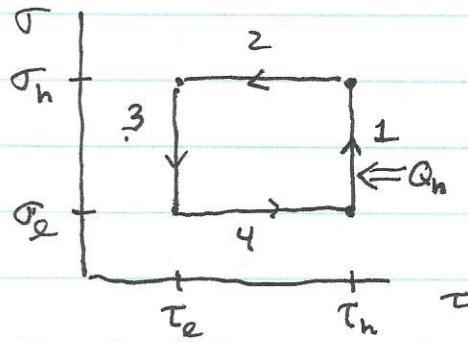
$$\Delta W_{\text{on}} \geq (T_h - T_e) \bar{T}_e = \left( \frac{T_h - T_e}{T_e} \right) Q_e$$

$$\left( \frac{\text{heat extracted}}{\text{work in}} \right) = \left( \frac{Q_e}{\Delta W_{\text{on}}} \right) \leq \frac{T_e}{T_h - T_e} = \eta_c \quad (0 < \eta_c < \infty !)$$

$$\eta \leq \eta_c$$

heat pump: (inside)  $\leftrightarrow$  (outside)

## Carnot cycle



1st Law

$$\Delta U = \int dU = \int dQ$$

$$\int \tilde{Q} = -\int \tilde{W} = \Delta W_{by}$$

$$\begin{aligned}\Delta W_{by} &= \int \tau d\sigma = T_h(\sigma_h - \sigma_l) + T_l(\sigma_l - \sigma_h) \\ &= (T_h - T_l)(\sigma_h - \sigma_l) \quad (\text{area of rect.})\end{aligned}$$

$$Q_h = T_h(\sigma_h - \sigma_l) = \text{heat in}$$

$$\therefore \left( \frac{\text{work out}}{\text{heat in}} \right) = \left( \frac{T_h - T_l}{T_h} \right) = \eta_c$$

max. efficiency : cyclic processes never truly reversible

Ideal gas cycle :  $\eta = \eta_c$

$$dU = \tilde{W} + \tilde{Q}$$

When can we write  $\tilde{Q} = dQ$  ~~and~~ or  $\tilde{W} = dW$ ?

If  $\tilde{Q} = dQ$  ~~or~~  $\tilde{W} = dW$  then If  $\tilde{Q}$  is exact so is  $\tilde{W}$ , and if  $\tilde{W}$  is exact so is  $\tilde{Q}$

$$1. \quad dU = \tilde{W} + dQ \Rightarrow \tilde{W} = d(U-Q) \equiv dW \quad (\text{i.e. if one is exact, so is the other!})$$

$\tilde{W}$  and  $\tilde{Q}$  are both exact

$$dU = dW + \tilde{Q} \Rightarrow \tilde{Q} = d(U-W) \equiv dQ$$

$$2. \quad \Delta Q = \int_1^2 \tilde{Q} = Q_2 - Q_1 \quad \text{and} \quad \Delta W = \int_1^2 \tilde{W} = W_2 - W_1$$

$$3. \quad \oint \tilde{Q} = 0 \quad \text{and} \quad \oint \tilde{W} = 0$$

### Isothermal work

$$\tilde{Q}_2 = \tau d\sigma = d(\tau\sigma) = dQ_\tau \Rightarrow dW = d(U-Q_\tau) = (dF)_\tau$$

$$\therefore F = \text{isothermal work, for } \tau = \text{const.} \quad (dU)_\tau = (dF)_\tau + (dQ)_\tau$$

### Isobaric work

$$-pdV = -d(pV) = d\sigma \quad (\Sigma \equiv F - \mu N)$$

$$\tilde{W} = -pdV + \tilde{W}' \quad (\tilde{W}' \equiv f_i dX_i) \quad \tilde{W}_p = -d(pV) + \tilde{W}'_p = d\sigma + \tilde{W}'_p$$

$$(dU)_p = \tilde{W}' - d(pV) + (Q_p) \quad \text{or} \quad (d(U+pV))_p = (dH)_p = \tilde{W}' + \tilde{Q}_p$$

$$H \equiv \text{enthalpy} \quad \tilde{W}' = 0 \Rightarrow (dH)_p = \tilde{Q}_p \quad \text{(evaporation from open vessel)}$$

at constant  $p$ , change in  $H = \tilde{W}' + \tilde{Q}_p$  is independent of volume-related work

### Isobaric, isothermal work

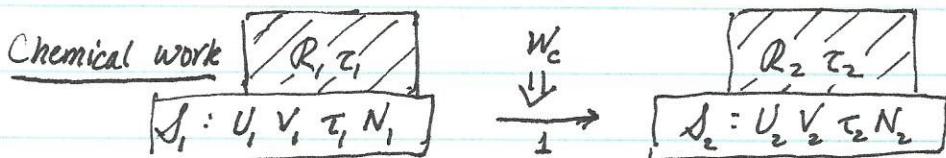
$$\tilde{Q} = d(\tau\sigma) = dQ_\tau \quad (d(U+pV))_{\tau p} = \tilde{W}' + dQ_\tau$$

$$\tilde{W}_p = -d(pV) + \tilde{W}'_p$$

$$\Rightarrow \tilde{W}' = (d(U+pV-Q_\tau))_{\tau p} \equiv (d(U+pV-\tau\sigma))_{\tau p}$$

Chemical reactions

$$\tilde{W}' = (dG)_{\tau p} \equiv \sum_i \mu_i dN_i$$



transfer one particle from  $S_1$  to  $S_2$  with  $(V_1, V_2)$  both constant,  $(T_1, T_2)$  const.

$$W_c = \mu_1(-1) + \mu_2(+1) = \mu_2 - \mu_1 = \text{chemical work done per particle}$$

$$\tilde{W}_c = \mu dN = (dG)_{SP}$$

Systems at constant volume - chemical, magnetic, electrical work per unit volume

$$\tilde{W} = \frac{\tilde{W}'}{V} = \mu d(\frac{N}{V}) + \tilde{W}_{mag} + \tilde{W}_{elec} \quad (\text{volume-independent work/vol.})$$

$$\tilde{W}_{mag} = d(\frac{1}{2}\mu_0 H^2) + \mu_0 \vec{H} \cdot d\vec{M} = \vec{H} \cdot d\vec{B} \quad \vec{B} \equiv \mu_0(\vec{H} + \vec{M})$$

$$\tilde{W}_{elec} = d(\frac{1}{2}\epsilon_0 E^2) + \vec{E} \cdot d\vec{P} = \vec{E} \cdot d\vec{D} \quad \vec{D} \equiv \epsilon_0 \vec{E} + \vec{P}$$

$(\vec{H}, \vec{E} \equiv \text{applied fields})$

$$d(\frac{U}{V}) \equiv du = \tilde{Q}_V + \tilde{W}'_V = \tau ds + \mu dn + \vec{H} \cdot d\vec{B} + \vec{E} \cdot d\vec{D}$$

$(\lambda \equiv \frac{\sigma}{V})$

$$F_V = f = u - \tau s$$

$$df = -sds + \mu dn + \vec{H} \cdot d\vec{B} + \vec{E} \cdot d\vec{D}$$

constant n, magnetic field case

$$df = -sds + \vec{H} \cdot d\vec{B}$$

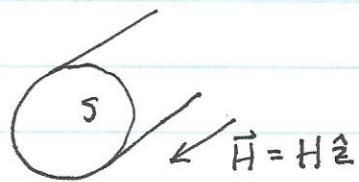
control  $\vec{H}$  (applied) not  $\vec{B}$  so use

$$g \equiv f - \vec{H} \cdot \vec{B} \quad dg = df - d(\vec{H} \cdot \vec{B}) = -sds - \vec{B} \cdot d\vec{H}$$

$$\Delta = -\left(\frac{\partial g}{\partial H_i}\right) \quad \vec{B} = -\left(\frac{\partial g}{\partial H_i}\right)_s$$

Example: superconductor in a magnetic field

$$\vec{B} = \mu_0(\vec{H} + \vec{M}) = 0 \text{ in } S \text{ (Meissner effect)}$$



superconducting cylinder in axial field

(to avoid demag factors)

For  $H=0$ ,  $S \rightarrow$  normal state at  $T=T_c$ .

At  $H_c(T)$   $S \rightarrow$  normal state

$$\text{Measurements: } H_c(T) = H_c(0) \left[ 1 - \left( \frac{T}{T_c} \right)^2 \right]$$

1. What is the decrease in energy upon going into the  $S$  state?

2. How does the specific heat behave at and below  $T_c$ ?

Just by knowing  $H_c(T)$  we can answer both of these questions

$T = \text{constant}$

$$g(T, H) - g(T, 0) = - \int_0^H B(H') dH'$$

$$\text{In normal (n) state } \vec{B} = \mu_0 \vec{H} \quad (\vec{M} = 0)$$

$$g_n(T, H) - g_n(T, 0) = -\frac{1}{2} \mu_0 H^2 \quad (1)$$

$$\text{In superconducting (S) state, } \vec{B} = 0 \quad (\vec{M} = -\vec{H}) \text{ so}$$

$$g_s(T, H) - g_s(T, 0) = 0 \quad (2)$$

At  $H = H_c(T)$ ,  $n$  and  $S$  are in phase equilibrium:

$$g_s(T, H_c) = g_n(T, H_c) = g_n(T, 0) - \frac{1}{2} \mu_0 H_c^2 \quad \text{by (1)}$$

$$g_s(T, H_c) = g_s(T, 0) \quad \text{by (2)}$$

$$\therefore g_s(T, 0) = g_n(T, 0) - \frac{1}{2} \mu_0 H_c^2$$

since  $f_{S,n}(T, 0) = g_{S,n}(T, 0)$ , can also write

$$f_s(T, 0) = f_n(T, 0) - \frac{1}{2} \mu_0 H_c^2$$

free energy is lower in  $S$  state by  $\frac{1}{2} \mu_0 H_c^2 \equiv$  "condensation energy"

$$= \frac{1}{2} \mu_0 H_c(0)^2 \left[ 1 - \left( \frac{T}{T_c} \right)^2 \right]^2$$

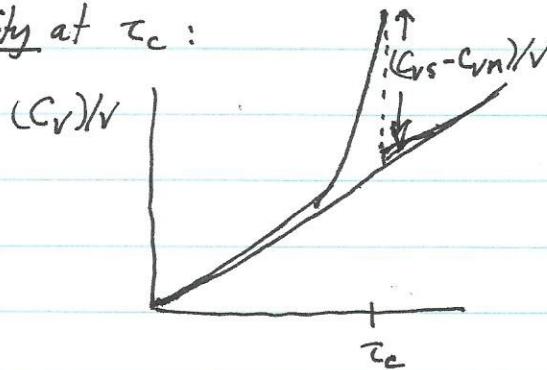
$$\Delta_s(\tau, 0) - \Delta_n(\tau, 0) = -\frac{\partial}{\partial \tau} (f_s(\tau, 0) - f_n(\tau, 0)) = \mu_0 H_c(\tau) \frac{dH_c}{d\tau}$$

$$C_V = T \left( \frac{\partial \sigma}{\partial T} \right)_V \Rightarrow V \tau \mu_0 \left[ \left( \frac{dH_c}{dT} \right)^2 + H_c(\tau) \frac{d^2H_c}{dT^2} \right] = C_{Vs} - C_{Vn}$$

There is a jump in specific heat at all  $\tau > 0$ .

$$\text{At } \tau = \tau_c \quad C_{Vs} - C_{Vn} = \left( V \tau \mu_0 H_c(0)^2 \frac{4\tau^2}{\tau_c^4} \right)_{\tau_c} = 4V \mu_0 H_c(0)^2 / \tau_c$$

Specific heat discontinuity at  $\tau_c$ :



Also

$$g_s(\tau, H) = g_s(\tau, 0) = g_n(\tau, 0) - \frac{1}{2} \mu_0 H_c^2$$

$$\begin{aligned} \Rightarrow g_s(\tau, H) - g_n(\tau, H) &= g_n(\tau, 0) - \frac{1}{2} \mu_0 H_c^2 - g_n(\tau, H) \\ &= \frac{1}{2} \mu_0 (H^2 - H_c^2) \end{aligned}$$

so, for  $H \neq 0$

$$\Delta_s - \Delta_n = \Delta_s(\tau, H) - \Delta_n(\tau, H) = \mu_0 H_c \frac{dH_c}{d\tau}$$

$$\Rightarrow C_H/V = T \left( \frac{\partial \Delta}{\partial T} \right)_H \Rightarrow (C_{sH} - C_{nH})/V = \mu_0 \tau \left[ \left( \frac{dH_c}{dT} \right)^2 + H_c \frac{d^2H_c}{dT^2} \right]$$

$\Rightarrow$  there is a jump in specific heat at all values of  $H$  (for  $\tau \neq 0$ ) : The

$$\left( (C_{sH} - C_{nH})/V = \mu_0 \tau \left[ \left( \frac{2H_{co}\tau}{\tau_c^2} \right)^2 + H_c(0) \left( 1 - \left( \frac{\tau}{\tau_c} \right)^2 \right) \left( \frac{-2H_{co}}{\tau_c^2} \right) \right] \right)$$

jump only  
depends on  $\tau$   
(cf. diagram  
above)

Exam 2 : 18 April - Friday

### Chemical Equilibria in Gases

$$G = U + PV - \tau\sigma = F + PV$$

$$dG = dU + d(PV) - d(\tau\sigma) = \tau d\sigma - PV + \sum_j \mu_j dN_j$$

where  $\tau\sigma$  is In equilibrium,  $G$  is min  $\Rightarrow dG = 0$ , so  $\frac{\partial G}{\partial P} = \frac{\partial G}{\partial \tau}$

$$(dG)_{T,P} = 0 = \sum_j \mu_j dN_j \quad (\text{sum over all species present})$$

$$(dU)_{T,P} = \tau d\sigma - PV + \sum_j \mu_j dN_j = d(\tau\sigma) - d(PV) + \sum_j \mu_j dN_j \quad (dG)_{T,P} = \sum_j \mu_j dN_j = 0$$

Consider



Stoichiometry requires

$$\Delta H_A = \frac{a}{b} \Delta H_B = -\frac{a}{c} \Delta H_C = -\frac{a}{d} \Delta H_D$$

$$\therefore \mu_A \Delta H_A + \mu_B \Delta H_B + \mu_C \Delta H_C + \mu_D \Delta H_D = 0$$

Take  $\Delta H_A = 1$ . Then

$$\Rightarrow a\mu_A + b\mu_B - c\mu_C - d\mu_D = 0$$

For an ideal gas

$$\mu_j = \tau \ln\left(\frac{n_j}{C_j}\right) \quad C_j \equiv n_{Qj} Z_j(\text{int}) = n_{Qj} e^{-F_j(\text{ext})/\tau} (2S_j + 1)$$

$$n_{Qj} \equiv \left(\frac{m_j \tau}{2\pi k T^2}\right)^{3/2}$$

$$\sum_j \mu_j v_j = \sum_j \tau \ln\left[\left(\frac{n_j}{C_j}\right)^{v_j}\right] = 0$$

$$\Rightarrow \prod_j \left(\frac{n_j}{C_j}\right)^{v_j} = 1 \quad \text{or} \quad \prod_j n_j^{v_j} = \prod_j C_j^{v_j} \equiv K(\tau)$$

$$\boxed{\prod_j (n_j)^{v_j} = K(\tau)} \quad \text{"Law of mass action"}$$

$$U = \tau\sigma - PV + \sum_j \mu_j dN_j$$

$$dU = \tau d\sigma - PV + \sum_j \mu_j dN_j \Rightarrow \sigma d\tau - V dp + \sum_j N_j d\mu_j = 0$$

$$dG = dU + d(PV) - d(\tau\sigma) = -\sigma d\tau + V dp + \sum_j \mu_j dN_j = \sum_j d(\mu_j N_j) \quad \checkmark$$

~~$$\sigma d\tau - V dp + (\mu_1 - \mu_2) dP + \sum_j (\mu_j^{(1)} - \mu_j^{(2)}) dN_j$$~~

### Dissociation of diatomic $H_2$



$$\gamma_{H_2} = 1 \quad \gamma_H = -2$$

$$\frac{n_{H_2}}{(n_H)^2} = K(\epsilon)$$

$$n_H = [H] \quad n_{H_2} = [H_2]$$

$$\Rightarrow \frac{[H]}{[H_2]} = \frac{1}{[H_2]^{\gamma_2} K(\epsilon)^{\gamma_2}}$$

lower  $[H_2] \Rightarrow$  higher  $\frac{[H]}{[H_2]}$   $\therefore$  lower density of  $[H_2]$  favors?

higher ratio  $\frac{[H]}{[H_2]}$  (as in interstellar space)

skip

pH



$$\frac{[H_2O]}{[H^+][OH^-]} = K(\epsilon) = \frac{[H_2O]}{10^{-14} (\text{mol}^2/\text{L}^2)} \text{ room } \epsilon$$

$$\text{pure } H_2O \quad [H^+] = [OH^-] = 10^{-7} \frac{\text{mol}}{\text{L}}$$

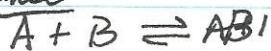
$$pH \equiv -\log_{10} [H^+]$$

$$\left\{ \begin{array}{ll} \cancel{pH} < 7 & \underline{\text{acid}} \\ pH > 7 & \underline{\text{base}} \end{array} \right.$$

oceans  $pH \sim 3$

human blood plasma  $pH \sim 7.3$  to  $7.5$

### Detailed Balance



$$\frac{dN_{AB}}{dt} = C n_A n_B - D n_{AB}$$

$\uparrow$  collision rate       $\uparrow$  decay rate

$$\text{Equilibrium } \frac{dN_{AB}}{dt} = 0 \Rightarrow \frac{n_A n_B}{n_{AB}} = \frac{D}{C} \quad (\text{e.g. } \frac{[H]^2}{[H_2]} = \frac{D}{C} = \frac{1}{K(\epsilon)})$$

$C n_A n_B = D n_{AB}$   $\leftarrow$  principle of detailed balance

## Nuclear abundances in early universe

$$Z_x \text{ p's} + N_x \text{ n's} \rightleftharpoons \text{nucleus } X : A_x = Z_x + N_x$$

$$Z_x \mu_p + N_x \mu_n = \mu_x$$

$$\mu_p = -\ln\left(\frac{n_p}{n_{ap} Z_p(\text{int})}\right) \quad \mu_n = -\ln\left(\frac{n_n}{n_{an} Z_n(\text{int})}\right) \quad \mu_x = -\ln\left(\frac{n_x}{n_{ax} Z_x(\text{int})}\right)$$

$$Z_p(\text{int}) = 2 e^{-m_p c^2 / T} \quad Z_n(\text{int}) = 2 e^{-m_n c^2 / T} \quad Z_x(\text{int}) = (2S_x + 1) e^{-M_x c^2 / T}$$

$$\left(\frac{n_p}{n_{ap}}\right)^{Z_x} \left(\frac{n_n}{n_{an}}\right)^{N_x} \bar{Z}_p^{-Z_x} \bar{Z}_n^{-N_x} = \frac{n_x}{n_{ax}} \bar{Z}_x^{-1}$$

or

$$n_x = n_{ax} Z_x \bar{Z}_p^{-Z_x} \bar{Z}_n^{-N_x} \left(\frac{n_p}{2n_{ap}}\right)^{Z_x} \left(\frac{n_n}{2n_{an}}\right)^{N_x} \quad (S_p = S_n = \frac{1}{2})$$

$$= (2S_x + 1) n_{ax} e^{-E_x^k / T} \left(\frac{n_p}{2n_{ap}}\right)^{Z_x} \left(\frac{n_n}{2n_{an}}\right)^{N_x}$$

$$\underline{T = 1 \text{ MeV}} \quad E_x^k \equiv M_x c^2 - Z_x m_p c^2 - N_x m_n c^2 = \text{nuclear binding energy}$$

$$\underline{\frac{n_p}{2n_{ap}}} = e^{-11.6} \quad \underline{\frac{n_n}{2n_{an}}} = e^{-7.6}$$

gives observed  $n_x$  up to  $A_x \sim 60$  to 70 ( $\rightarrow \text{Cu or Zn}$ )

For heavier elements  $n_x$  is too small compared to observed value.