

# Tilted window: ray propagation

- Calculate phase shift caused by the insertion of the window into an interferometer.
- Ray optics:
  - Add up optical path for each segment
  - Subtract optical path w/o window

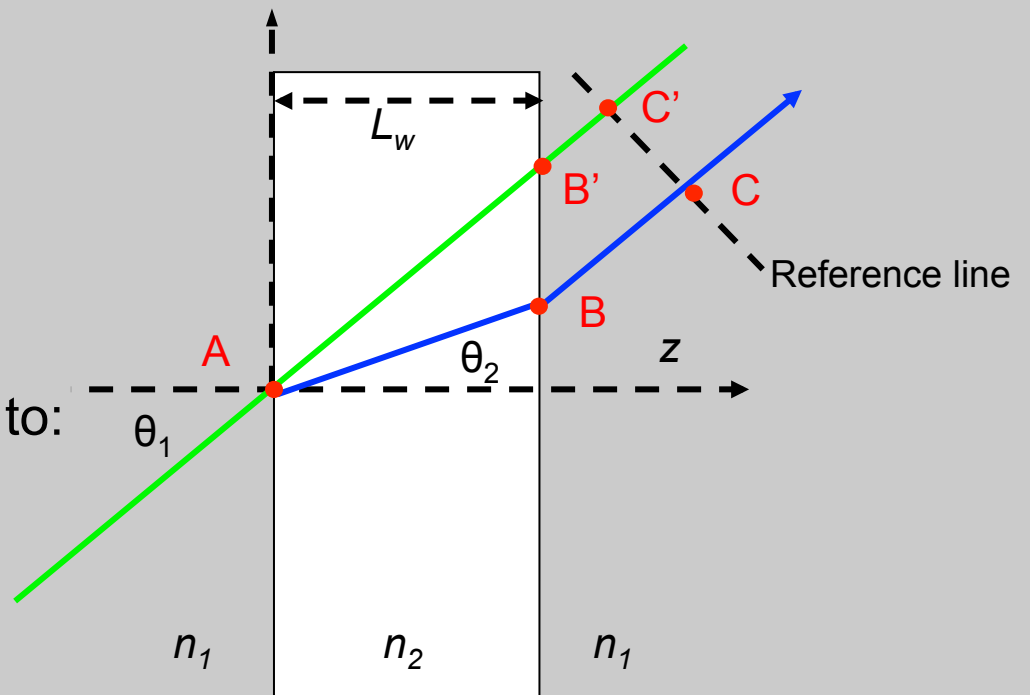
$$\Delta d = nL_{AB} + L_{BC} - L_{AB'} - L_{B'C'}$$

$$L_{AB} = \frac{L_w}{\cos\theta_2} \quad L_{AB'} = \frac{L_w}{\cos\theta_1}$$

$$L_{BC} = L_{B'C'} + L_{BB'} \sin\theta_1$$

- Use Snell's Law to reduce to:

$$\Delta d = nL_w \cos\theta_2 - L_w \cos\theta_1$$



# Tilted window: wave propagation

- Write expression for tilted plane wave

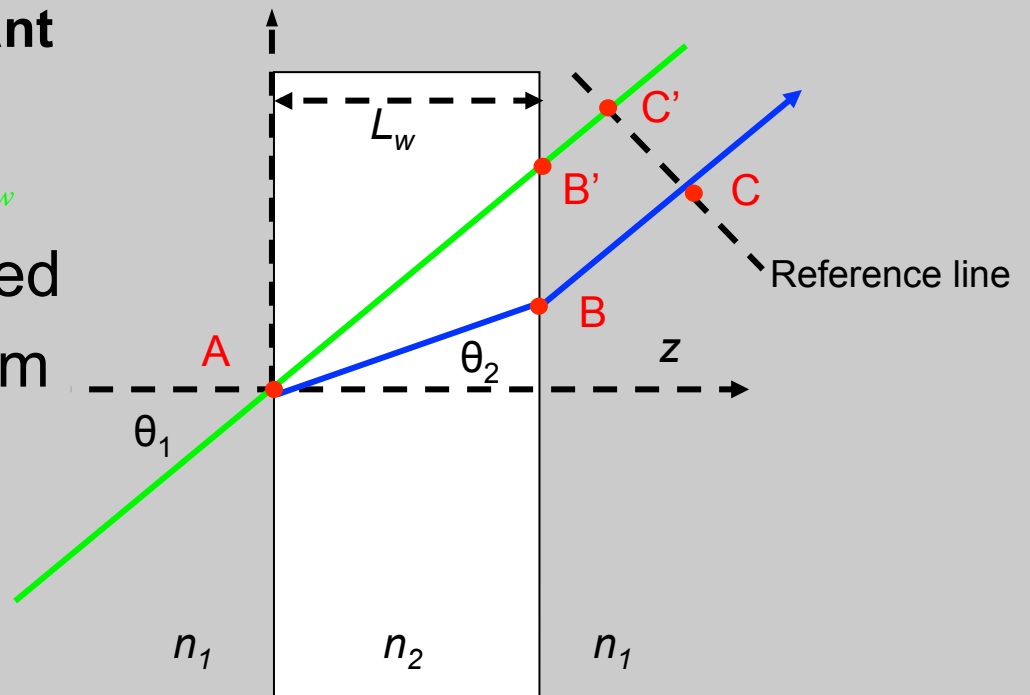
$$E(x,z) = E_0 \exp[i(k_x x + k_z z)] = E_0 \exp\left[i \frac{\omega}{c} n (x \sin \theta_2 + z \cos \theta_2)\right]$$

- Snell's Law: phase across surfaces is conserved

$$k_x x = \frac{\omega}{c} n \sin \theta \quad \text{is constant}$$

$$\Delta\phi = (k_2 \cos \theta_2) L_w - (k_1 \cos \theta_1) L_w$$

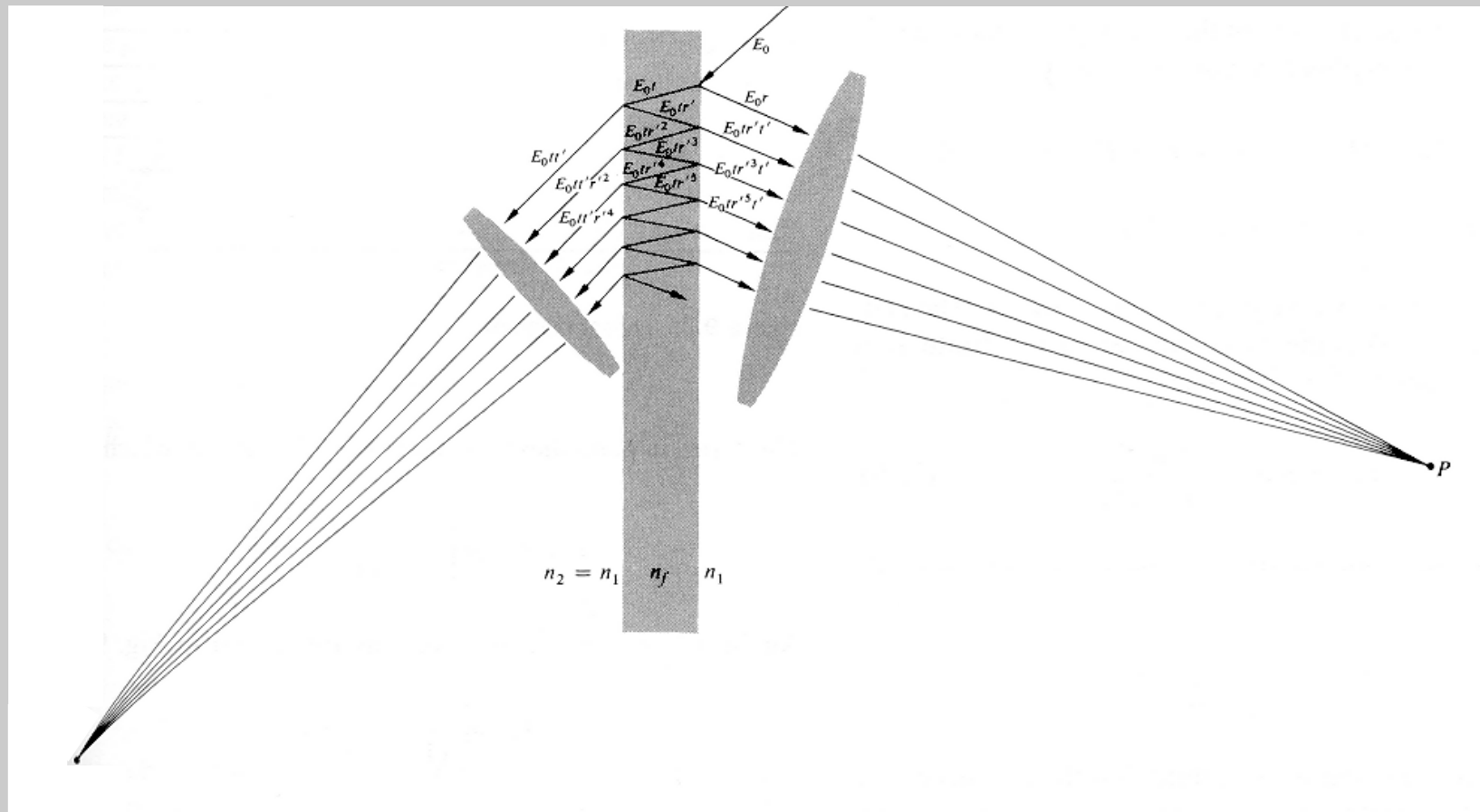
- This approach can be used to calculate phase of prism pairs and grating pairs



# Multiple-beam interference: The Fabry-Perot Interferometer or Etalon

A Fabry-Perot interferometer is a pair of **parallel** surfaces that reflect beams back and forth. An etalon is a type of Fabry-Perot etalon, and is a piece of glass with parallel sides.

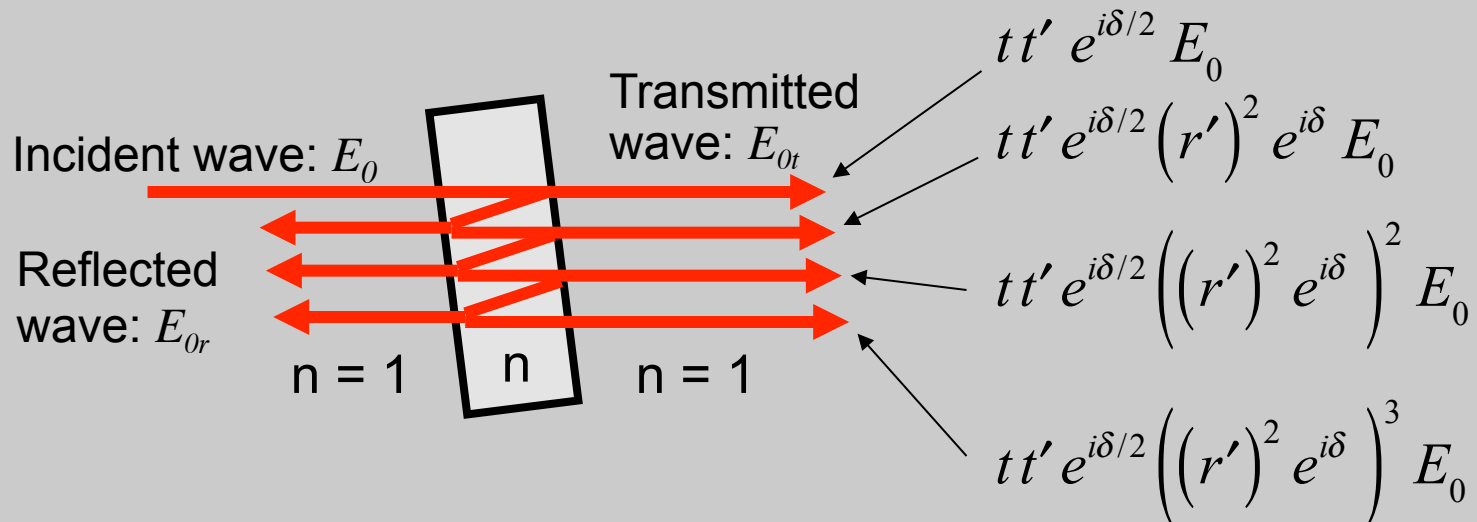
The transmitted wave is an infinite series of multiply reflected beams.



# Linear systems approach to the FP

- As with any linear device, we can represent its action in either the temporal or frequency domain
  - Frequency domain:  $H(\omega)$  = transfer function
  - Time domain:  $h(t)$  = impulse response
- First we will start with the conventional approach:
  - Incident monochromatic plane wave
  - Calculate transmitted amplitude and phase for  $H(\omega)$
- Then we should be able to calculate impulse response:
  - $h(t) = \text{FT}^{-1}\{ H(\omega) \}$

# Calculation of the FP frequency response



$r, t$  = reflection, transmission coefficients from air to glass  
 $r', t'$  = “ “ “ from glass to air

$\delta$  = round-trip phase delay inside medium =  $k_0(2 n L \cos \theta_t)$

$$\delta(\omega) = \omega \frac{2nL}{c} \cos \theta_t(\omega) \approx \omega \frac{2L}{c} \cos \theta_i \quad \text{for } n=1$$

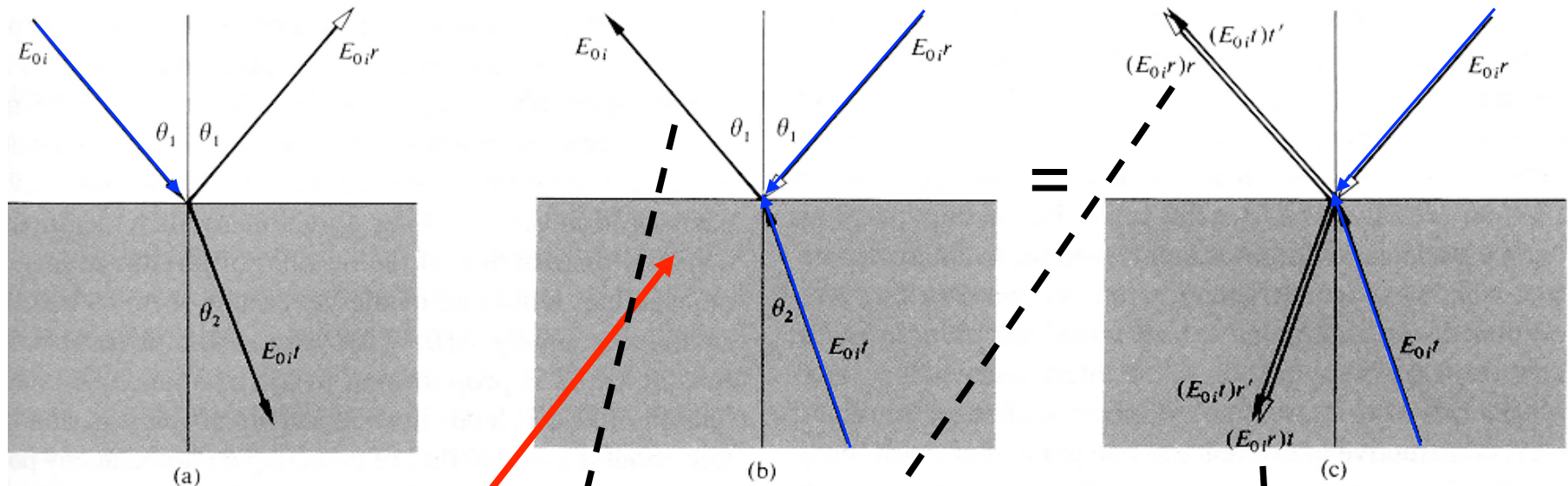
Transmitted wave:

$$E_{0t} = tt' e^{i\delta/2} E_0 \left( 1 + (r')^2 e^{i\delta} + \left( (r')^2 e^{i\delta} \right)^2 + \left( (r')^2 e^{i\delta} \right)^3 + \dots \right)$$

Reflected wave:

$$E_{0r} = rE_0 + tt'r'e^{i\delta} E_0 + tt'r' \left( (r')^2 e^{i\delta} \right)^2 E_0 + \dots$$

# Stokes relations for reflection and transmission



“Time reversal:”  
Same amplitudes,  
reversed propagation  
direction

$$E_{oi} = (E_{oi} r) r + (E_{oi} t) t'$$

$$\therefore tt' = 1 - r^2$$

$$(E_{oi} t) r' + (E_{oi} r) t = 0$$

$$\therefore r' = -r$$

## Notes:

- relations apply to angles connected by Snell's Law
- true for any polarization, but not TIR
- convention for which interface experiences a sign change can vary

# Fabry-Perot transfer function

Stokes' relations

$$r' = -r$$

$$r'^2 = r^2$$

$$tt' = 1 - r^2$$

The transmitted wave field is:

$$E_{0t} = tt'e^{i\delta/2} E_0 \left( 1 + (r')^2 e^{i\delta} + \left( (r')^2 e^{i\delta} \right)^2 + \left( (r')^2 e^{i\delta} \right)^3 + \dots \right)$$

$$= tt'e^{i\delta/2} E_0 \left( 1 + r^2 e^{i\delta} + \left( r^2 e^{i\delta} \right)^2 + \left( r^2 e^{i\delta} \right)^3 + \dots \right)$$

Perform sum over infinite series:

Let

$$x = r^2 e^{i\delta} \quad E_{0t} = tt'e^{i\delta/2} E_0 \sum_{m=0}^{\infty} (r^2 e^{i\delta})^m = (1 - r^2) e^{i\delta/2} E_0 \sum_{m=0}^{\infty} x^m$$

For  $|x| < 1$ :

$$\sum_{m=0}^{\infty} x^m = 1 + x + x^2 + x^3 + \dots = (1 - x)^{-1}$$

$$\Rightarrow E_{0t} = E_0 \frac{(1 - r^2) e^{i\delta/2}}{1 - r^2 e^{i\delta}} = E_0(\omega) \frac{(1 - r^2) \exp \left[ i\omega \frac{L}{c} \cos \theta_i \right]}{1 - r^2 \exp \left[ i\omega \frac{2L}{c} \cos \theta_i \right]} \equiv E_0(\omega) H(\omega)$$

# FP impulse response

- Simple case:  $n = 1$ , normal incidence

$$H(\omega) = \frac{(1-r^2) \exp\left[i\omega \frac{L}{c} \cos\theta_i\right]}{1-r^2 \exp\left[i\omega \frac{2L}{c} \cos\theta_i\right]} \rightarrow \frac{1-r^2}{1-r^2 e^{i\omega T_{RT}}}$$

Dropping common term:  
 $e^{i\omega T_{RT}/2}$   
 $T_{RT} = 2L / c$

- $FT^{-1}$  to get impulse response

$$H(\omega) = \frac{1-r^2}{1-r^2 e^{i\omega T_{RT}}} = (1-r^2) \sum_{m=0}^{\infty} (r^2 e^{i\omega T_{RT}})^m$$

$$h(t) = FT^{-1}\{H(\omega)\} = (1-r^2) \sum_{m=0}^{\infty} r^{2m} FT^{-1}\{e^{im\omega T_{RT}}\}$$

$$h(t) = (1-r^2) \sum_{m=0}^{\infty} r^{2m} \delta(t - m\omega T_{RT})$$



# High reflectivity limit

- When the reflectivity is high, very little is transmitted through the output on each reflection

$$r^2 = R \quad \text{Power reflectivity}$$

Logarithmic cavity loss  
(single pass)

$$R^m = (1 - T)^m \approx (1 - mT) \approx e^{-2m\gamma}$$

$$\gamma = -\ln T = -\ln(1 - R)$$

- We can represent this as a time dependent loss function:

$$L(t) = e^{-t/\tau_c}$$

$$\text{Cavity lifetime: } \tau_c = T_{RT} / 2\gamma$$

$$h(t) = (1 - r^2) \sum_{m=0}^{\infty} r^{2m} \delta(t - m\omega T_{RT}) \rightarrow (1 - r^2) \Theta(t) e^{-t/\tau_c} \text{comb}(t / T_{RT})$$

# Another calculation of the transfer function

- With this low cavity loss representation of the impulse response, FT to get to  $H(\omega)$

$$h(t) = (1 - r^2) \Theta(t) e^{-t/\tau_c} \text{comb}(t / T_{RT}) = (1 - r^2) f(t) g(t)$$

$$H(\omega) = FT \{ h(t) \} = (1 - r^2) \frac{1}{2\pi} F(\omega) \otimes G(\omega)$$

$$F(\omega) = \int_0^{\infty} e^{-t/\tau_c} e^{i\omega t} dt = \frac{e^{-t/\tau_c + i\omega t}}{-1/\tau_c + i\omega} \Big|_0^{\infty} = \frac{1}{1/\tau_c - i\omega} \quad \text{Complex Lorentzian}$$

$$G(\omega) = FT \{ \text{comb}(t / T_{RT}) \} = \frac{2\pi}{T_{RT}} \text{comb} \left( \frac{\omega}{2\pi / T_{RT}} \right)$$

# Fabry-Perot power transmission

$$E_{0t} = E_0 \frac{1-r^2}{1-r^2 e^{i\delta}} e^{i\delta/2}$$

Power transmittance:  $T \equiv \left| \frac{E_{0t}}{E_0} \right|^2 = \left| \frac{(1-r^2)e^{i\delta/2}}{1-r^2 e^{i\delta}} \right|^2 = \frac{(1-r^2)^2}{(1-r^2 e^{+i\delta})(1-r^2 e^{-i\delta})}$

$$= \left[ \frac{(1-r^2)^2}{\{1+r^4-2r^2 \cos(\delta)\}} \right] = \left[ \frac{(1-r^2)^2}{\{1+r^4-2r^2[1-2\sin^2(\delta/2)]\}} \right] = \left[ \frac{(1-r^2)^2}{\{1-2r^2+r^4+4r^2 \sin^2(\delta/2)\}} \right]$$

Dividing numerator and denominator by  $(1-r^2)^2$

$$T = \frac{1}{1+F \sin^2(\delta/2)}$$

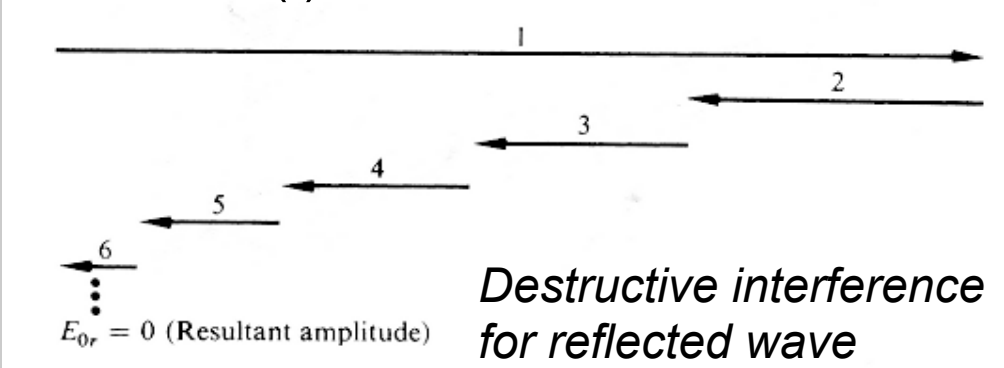
where:  $F = \left[ \frac{2r}{1-r^2} \right]^2$

# Multiple-beam interference: simple limits

## Reflected waves

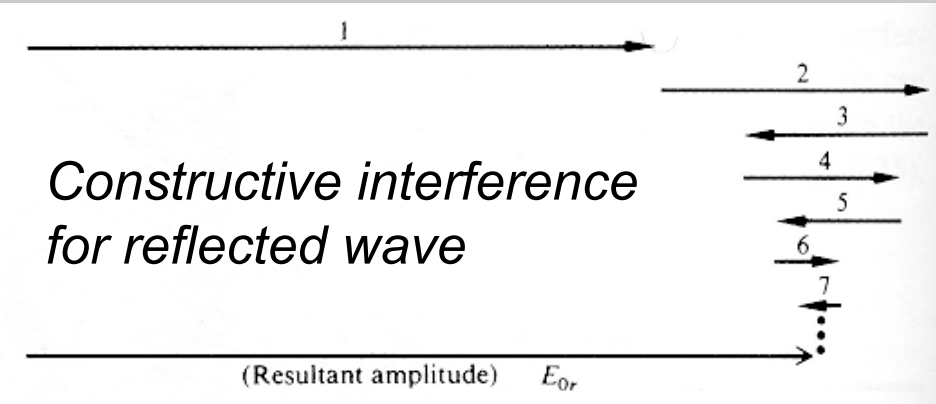
$$T = \frac{1}{1 + F \sin^2(\delta / 2)}$$

Full transmission:  $\sin(\delta) = 0, d = 2 \pi m$

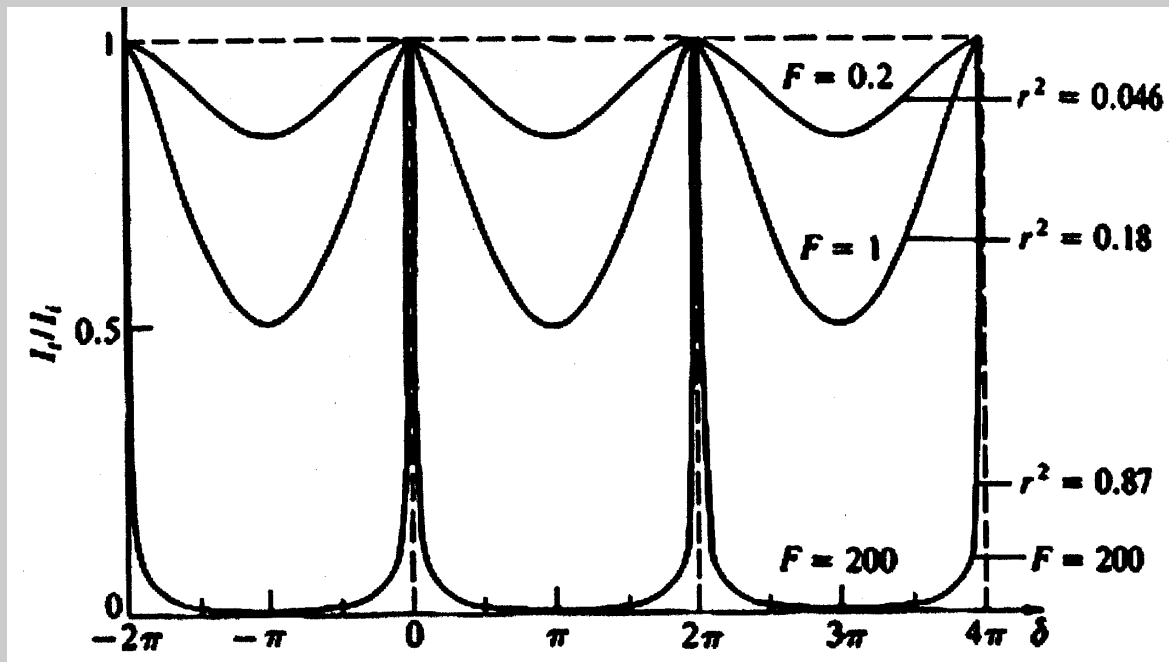


1st reflection  
internal reflections

Minimum transmission:  $\sin(\delta) = 1, d = 2 \pi (m + 1/2)$



# Etalon transmittance vs. thickness, wavelength, or angle



$$T = \frac{1}{1 + F \sin^2(\delta / 2)}$$

Transmission max:  
 $\sin(\ ) = 0$ ,  $d = 2 \pi m$

$$\delta = \frac{\omega}{c} 2 n L \cos[\theta_t]$$

$$= 2 \pi m$$

At normal incidence:

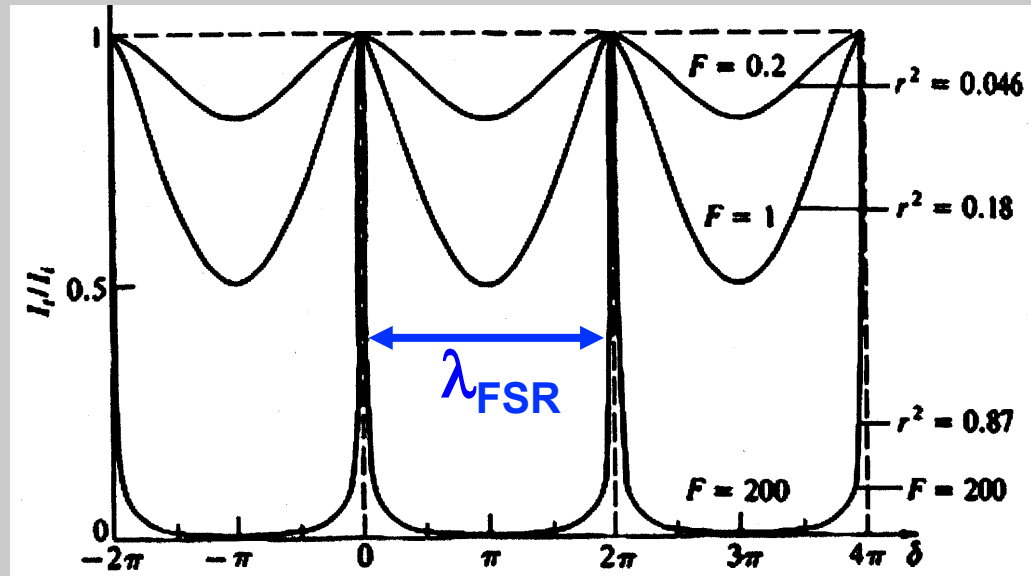
$$\lambda_m = \frac{2 n L}{m} \quad \text{or} \quad n L = m \frac{\lambda_m}{2}$$

- The transmittance varies significantly with thickness or wavelength.
- We can also vary the incidence angle, which also affects  $\delta$ .
- As the reflectance of each surface ( $R=r^2$ ) approaches 1, the widths of the high-transmission regions become very narrow.

# The Etalon Free Spectral Range

The Free Spectral Range is the wavelength range between transmission maxima.

$$\lambda_{FSR} = \text{Free Spectral Range}$$



For neighboring orders:

$$\frac{4\pi nL}{\lambda_1} - \frac{4\pi nL}{\lambda_2} = 2\pi \Rightarrow \frac{1}{\lambda_1} - \frac{1}{\lambda_2} = \frac{1}{2nL} = \frac{\lambda_2 - \lambda_1}{\lambda_1 \lambda_2}$$

$$\lambda_2 - \lambda_1 = \lambda_{FSR}$$

$$\lambda_2 \lambda_1 \approx \lambda^2$$

$$\lambda_{FSR} \approx \frac{\lambda^2}{2nL}$$

$$\frac{\lambda_{FSR}}{\lambda} = \frac{\lambda}{2nL} = \frac{\nu_{FSR}}{\nu}$$

$$\nu_{FSR} \approx \frac{c}{2nL}$$

1/(round trip time)

# Etalon Linewidth

The **Linewidth**  $\delta_{LW}$  is a transmittance peak's full-width-half-max (FWHM).

$$T = \frac{1}{1 + F \sin^2(\delta / 2)}$$

A maximum is where  $\delta / 2 \approx m\pi + \delta' / 2$  and  $\sin^2(\delta / 2) \approx \delta' / 2$

Under these conditions (near resonance),

$$T = \frac{1}{1 + F\delta'^2 / 4}$$

This is a Lorentzian profile, with FWHM at:

$$\frac{F}{4} \left( \frac{\delta_{LW}}{2} \right)^2 = 1 \Rightarrow \delta_{LW} \approx 4 / \sqrt{F}$$

This transmission linewidth corresponds to the minimum resolvable wavelength.

# Etalon Finesse

The Finesse,  $\mathfrak{F}$ , is the ratio of the Free Spectral Range and the Linewidth:

$$\mathfrak{F} \equiv \frac{\delta_{FSR}}{\delta_{FW}} = \frac{2\pi}{4/\sqrt{F}} = \frac{\pi\sqrt{F}}{2}$$

$\delta = 2\pi$  corresponds to one FSR

Using:  $F = \left[ \frac{2r}{1-r^2} \right]^2$

$$\mathfrak{F} = \frac{\pi}{1-r^2}$$

taking  $r \approx 1$

The Finesse is the number of wavelengths the interferometer can resolve.