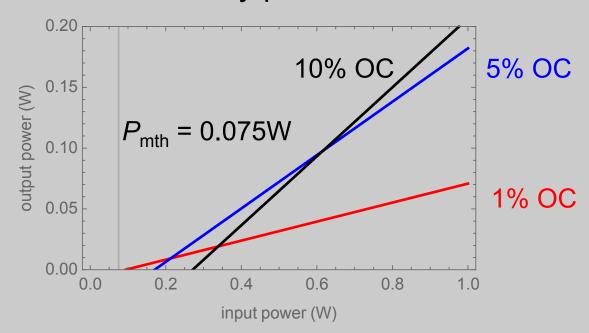
# Optimizing output coupling

- As output coupling increases
  - pump threshold decreases
  - Fraction of intracavity power transmitted increases



 $-P_{mth}$  = threshold for lasing when there is no output coupling

## Minimum pump threshold

 The threshold power and slope efficiency both depend on the amount of output coupling loss

$$P_{out} = I_s A_b \frac{\gamma_2}{2} \left( \frac{P_p}{P_{th}} - 1 \right) \qquad P_{th} = I_s A_p \frac{\gamma}{\eta_p} \frac{h v_p}{h v_{21}} \qquad \gamma = \gamma_i + \frac{1}{2} \gamma_1 + \frac{1}{2} \gamma_2$$

- Lower output coupling leads to low threshold power, but less is let out of the cavity
- Define  $P_{mth}$  = minimum threshold power, with **no** output coupling

$$P_{mth} = I_s A_p \frac{\gamma_i + \frac{1}{2} \gamma_1}{\eta_p} \frac{h \nu_p}{h \nu_{21}} \longrightarrow P_{th} = P_{mth} \left( 1 + \frac{\frac{1}{2} \gamma_2}{\gamma_i + \frac{1}{2} \gamma_1} \right)$$

Define ratio of pump power to minimum threshold pump power:

$$x_m = \frac{P}{P_{mth}}$$

# Output power vs OC transmission

 Define a parameter S, which is the ratio of OC loss to other losses

$$P_{th} = P_{mth} \left( 1 + \frac{\frac{1}{2} \gamma_2}{\gamma_i + \frac{1}{2} \gamma_1} \right) \equiv P_{mth} \left( 1 + S \right)$$

Now look at output power vs S

$$P_{out} = I_s A_b \frac{\gamma_2}{2} \left( \frac{P_p}{P_{th}} - 1 \right)$$

$$= I_s A_b \frac{\gamma_2}{2} \left( \frac{P_p}{P_{mth}} - 1 \right)$$

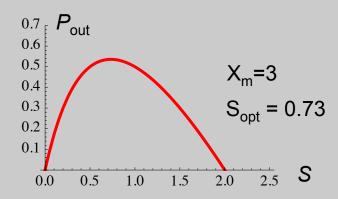
$$= I_s A_b \left( \gamma_i + \frac{1}{2} \gamma_1 \right) S \left( \frac{x_m}{(1+S)} - 1 \right)$$

$$P_{\text{mth}}^{4} = \frac{1}{2} \frac{1$$

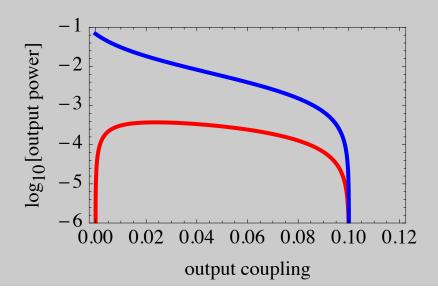
# **Optimized OC transmission**

- Output power maximizes:
  - Low OC transmission, no output
  - High OC transmission, high P<sub>th</sub>
- Find OC for maximum:

- set 
$$\partial_S P_{out}(S) = 0$$
  
 $S_{opt} = \sqrt{x_m} - 1$ 



Intracavity power decreases with greater output coupling



$$P_{\rm int} = P_{out} / \gamma_2$$

Intracavity power is always higher than output power

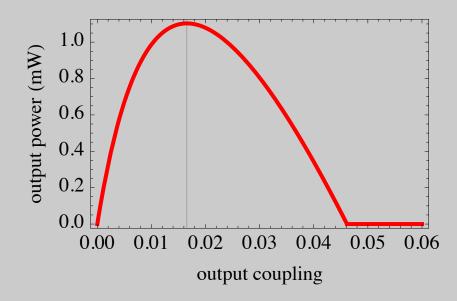
# **Example: HeNe laser**

#### Laser parameters

$$\lambda_1 = 632.8 nm$$
  $hv_{21} = 1.86 eV$ 

$$\sigma_{21} = 3 \times 10^{-15} \,\mathrm{cm}^2$$
  $\tau_{21} = 150 \,\mathrm{ns}$ 

$$\Gamma_{sat} = \frac{hv_{21}}{\sigma_{21}} = 1\mu\text{J/cm}^2$$
  $I_{sat} = \frac{\Gamma_{sat}}{\tau_{21}} = \frac{hv_{21}}{\sigma_{21}\tau_{21}} = 6.6\text{W/cm}^2$ 



Assume uniform pump and laser mode

$$d_{\text{pump}}$$
=2mm  $D_{\text{mode}}$ =1.75mm

$$\gamma_p=1\%$$
 Min. threshold pump power:  $P_{mth}=2mW$ 

$$L_{\text{cavity}}$$
=40cm  $T_{\text{RT}}$ =2.7ns

Cavity photon lifetime at opt. OC:  $\tau_c$ =72.5ns

Effective input pump power:  $P_p=7mW$ 

Best slope efficiency, relative to effective input pump power:  $\eta_s$ =0.35

Lamp pumping

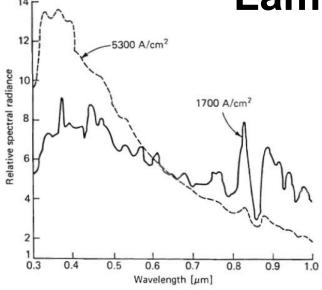
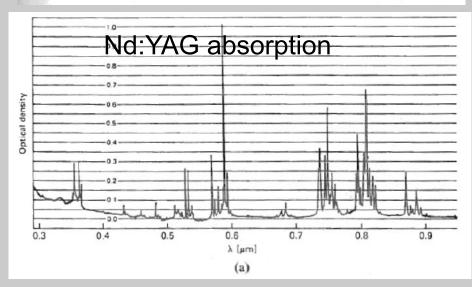
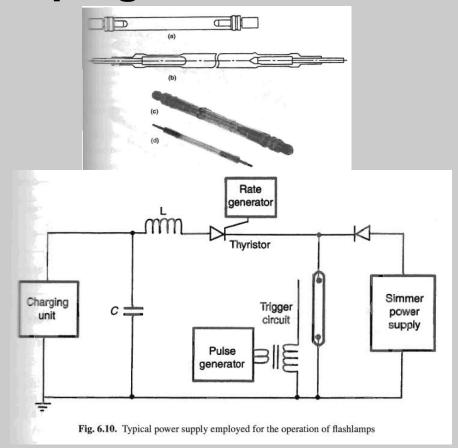


Fig. 6.3. Spectral emission of a xenon flash tube (EG&G, model FX-47A) operated at high current densities. Lamp fill pressure is 0.4 atm. The spectrum at the two current densities can be approximated by blackbodies = 7000 and 9400 K, respectively [6.1]





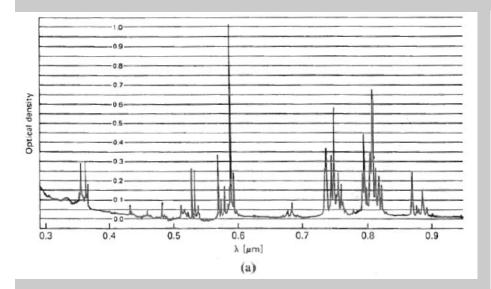
#### Account for:

- Efficiency of converting electrical to optical power
- spectral overlap efficiency

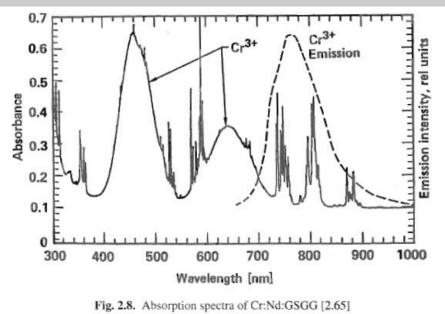
# Improving spectral overlap

 Can sensitize material to absorb, then transfer to ions for better inversion density

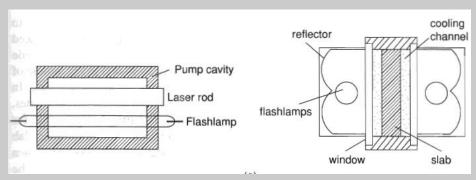




#### Cr:Nd:GSGG



## **Pump chambers**

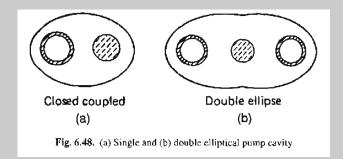


Components of the first ruby laser

100% reflective mirror Quartz flash tube
Ruby crystal

Polished aluminum reflecting cylinder 95% reflective mirror

 Couple optical output from lamp into laser crystal



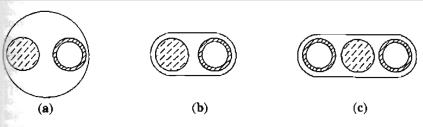
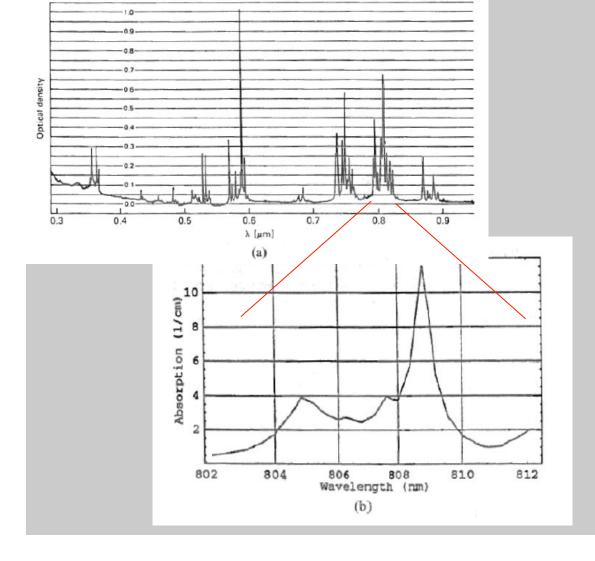


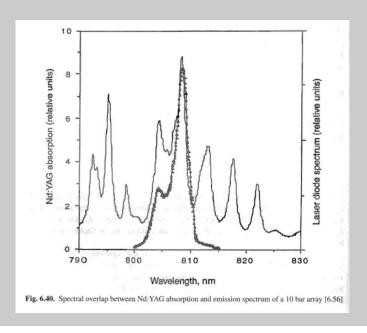
Fig. 6.49. Nonfocusing pump cavities; (a) circular cylinder, (b) single, and (c) double-lamp closed-coupled configuration

Account for pump transfer efficiency

# **Diode pumping**

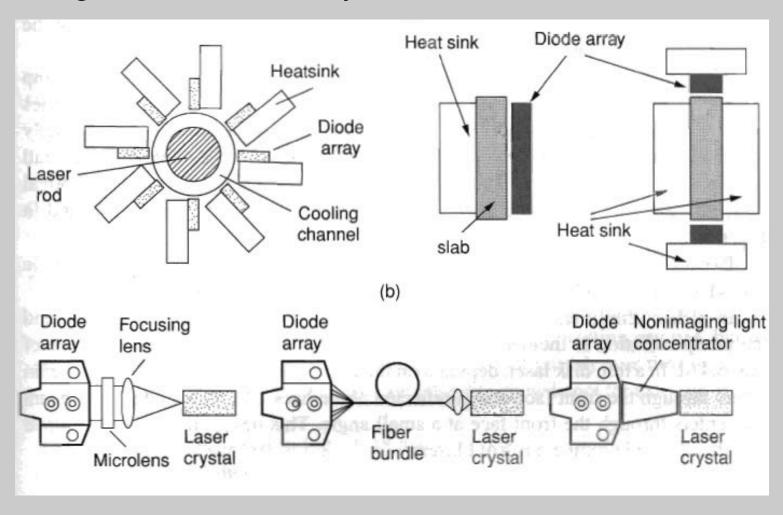
Pump at strong absorption line near 808nm



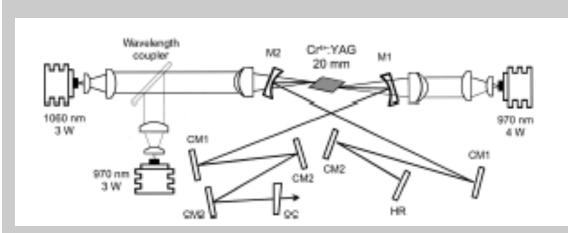


# Diode pumping configurations

Single emitters or arrays



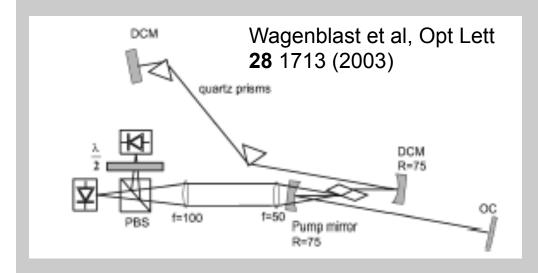
## **Direct-diode pumped KLM lasers**



Cr<sup>4+</sup>:YAG

8.3W pump, 10mW avg out 65fs pulse Double-sided, 2 wavelength pumping

Naumov et al, Opt Lett v29 1276 (2004)

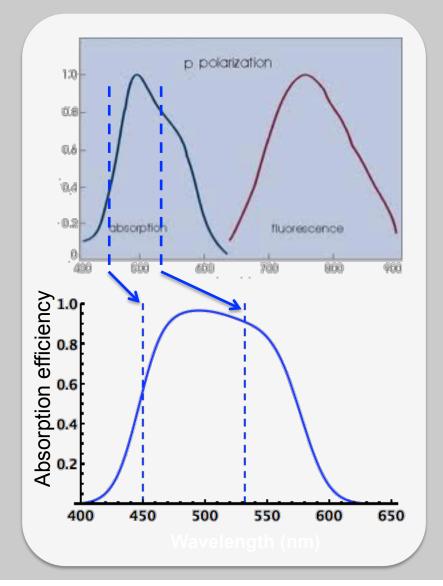


#### Cr<sup>3+</sup>:LiCAF

1.0W pump, 40mW avg out10fs pulsePolarization-multiplexed pumping

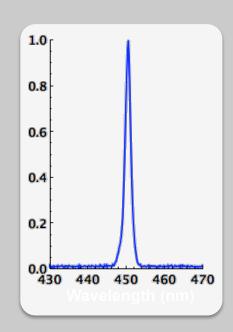
# Challenges to diode-pumping Ti:sapphire

- Desire small pump mode volume
  - Efficiency
  - Soft-aperture for Kerr-lens modelocking
- Pump absorption efficiency
- Quantum defect

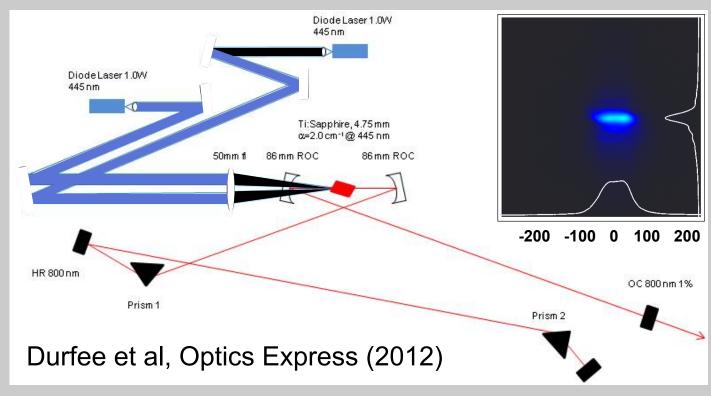


## High-power blue laser diodes

- GaN based diodes
- Used commercially for projectors
- Facet: 15:1 aspect ratio
- Fast/slow axis divergence: ~3.5:1
- 1.2, 1.6, 2 watts/single emitter now available
- 445nm typical, some lot variation
- Small shift in output wavelength with temperature.



# **Cavity layout**



#### Pump optics:

- Asphere + 3:1 cylindrical telescope
- Side-by-side beams

#### Laser cavity designed for low threshold

- 86mm ROC curved mirrors for smaller intracavity mode size
- 1% OC for higher intracavity power
- Green pump: 30mW mode-locked with 500mW pump power

## **Laser operation**

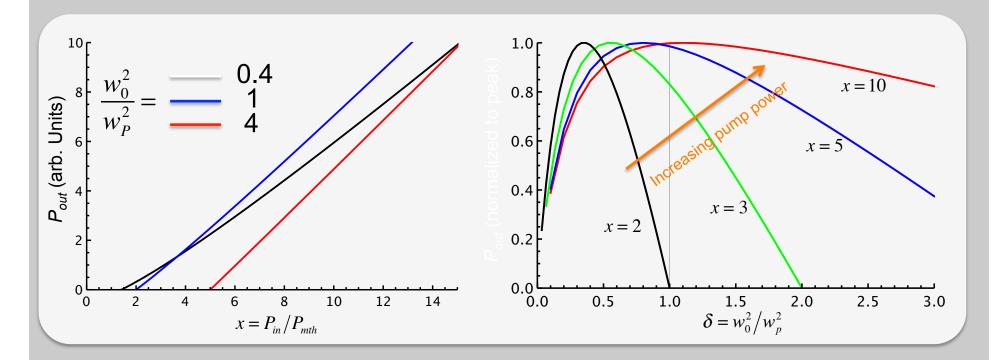


1.8W to crystal, 60% absorption Average output power:

- 40mW optimized CW
- 32mW mode-locked

### **Contributions to KLM**

- Soft aperture in vertical direction
- Uniform gain along optical axis (60% pump absorption)
- Re-imaging of CW and ML spots shows z-shift in waist location.
- Low-threshold operation for small mode size gives high discrimination



# 4-level system comparison: Nd:YAG

#### Assume:

- 1W pump available, aim for P<sub>th</sub>=100mW
- Thickness or concentration in gain medium enough to fully absorb pump
- 5% OC

#### Nd:YAG

$$\sigma_{21} = 2.8 \times 10^{-19} cm^2$$
  $\Gamma_{sat} = 0.63 J / cm^2$   $\lambda_L = 1064 nm$   $I_{sat} = 2751 W / cm^2$   $\omega_P = 140 \mu m$   $\lambda_P = 808 nm$   $\eta_S = 76\%$   $\sigma_{21} = 230 \mu s$