

Birefringent phase matching

It is clear from the solutions of the coupled wave eqns. that high efficiency requires

$$\Delta k = k_1 + k_2 - k_3 = 0$$

When $\Delta k \neq 0$ the yield varies as $\text{sinc}^2(\Delta k L / 2)$

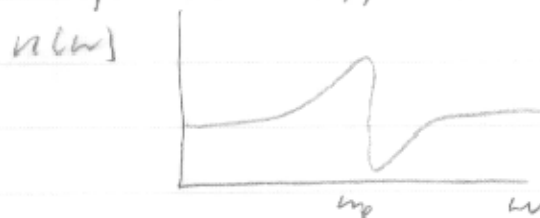
$\Delta k = 0$ sets a condition on the refr. index:

$$\Delta k = k_1 + k_2 - k_3 = n_1 \omega_1 + n_2 \omega_2 - n_3 \omega_3$$

as shown in book (2.7.7) this cannot take place with "normal" dispersion, where $n_3 > n_1, n_2$

techniques:

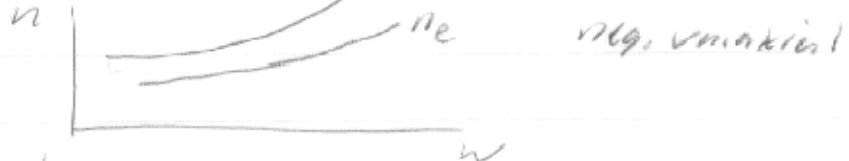
- anomalous dispersion: typ ω_3 on high side of resonance.



examples: mixing in gas (VUV)

HLIG

- birefringent PM



> angle-tune

> temperature tune.

- Quasi phase matching: periodic modulation at $\Delta k \neq 0$
→ slow buildup in signal

Wave propagation in birefringent media.
(non magnetic, no free charge)

$$\nabla \cdot \vec{D} = 0 \quad \nabla \cdot \vec{H} = 0$$

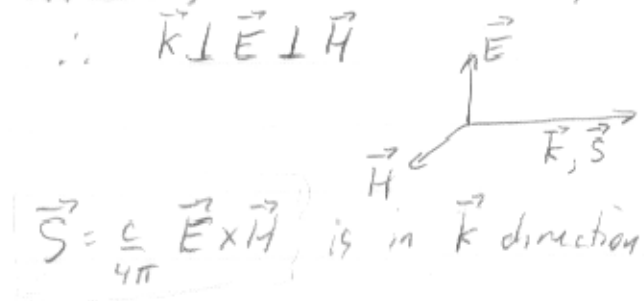
$$\nabla \times \vec{E} = -\frac{1}{c} \frac{\partial \vec{H}}{\partial t} \quad \nabla \times \vec{H} = \frac{1}{c} \frac{\partial \vec{D}}{\partial t}$$

all fields will share same time dependence $\sim e^{-i\omega t}$
 $\frac{\partial}{\partial t} \rightarrow -i\omega$

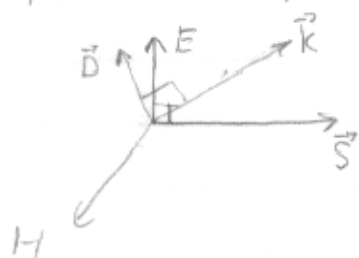
there will be a plane wave solution $\sim e^{i\vec{k} \cdot \vec{r}}$
 - don't know \vec{k} but can solve for it
 $\nabla \rightarrow i\vec{k}$

$$\rightarrow \vec{k} \times \vec{E} = \frac{\omega}{c} \vec{H} \quad \boxed{\vec{k} \times \vec{H} = -\frac{\omega}{c} \vec{D}}$$

in an isotropic medium, $\vec{D} = \epsilon \vec{E}$ and
 $\vec{H} \perp \vec{k}, \vec{E}$ $\vec{E} \perp \vec{k}, \vec{H}$
 $\therefore \vec{k} \perp \vec{E} \perp \vec{H}$



Anisotropic: $\vec{H} \perp \vec{k}, \vec{E}$ still $\vec{D} \perp \vec{H}$ also, but $\vec{D} \nparallel \vec{E}$



wavefronts are $\perp \vec{k}$
 power flows along \vec{S} : like "ray" in geom. optics

Birefringent case: most common by far.

2 options ω_1 is along lowest index direction.

Type I:

ω_1 and ω_2 share same polarization.

$$\vec{E}_1 \parallel \vec{E}_2$$

Type II:

$$\vec{E}_1 \perp \vec{E}_2$$

"Type III" also called 90° Phase matching.

- like Type I, but input at $\theta = 90^\circ$ and temperature tuned.

- LiNbO_3 most common.

Angle tuning:

via $n_e(\theta)$ function

$$\frac{1}{n_e(\theta)^2} = \frac{\sin^2 \theta}{n_e^2} + \frac{\cos^2 \theta}{n_o^2}$$

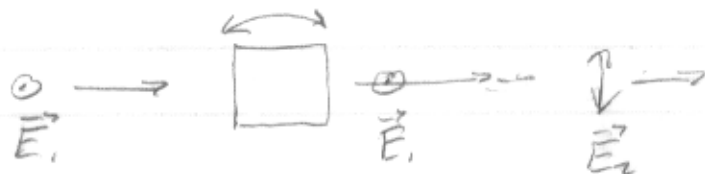
Ex Type I: neg. uniaxial

$$n_e(2\omega, \theta) = n_o(\omega)$$

input \vec{E}_1 along n_o , vary crystal angle around

\vec{E}_1 to tune index of ω_2

$$\vec{E}_2 \perp \vec{E}_1$$



practical concerns:

- cut crystal for the process
 - x-ray diff to get angle close
- protective A/R coating or in cell to keep off water.

Anisotropic media: birefringence.

in an isotropic medium:

$$\vec{D} = \epsilon \vec{E}$$

if linear, ϵ doesn't depend on \vec{E}


$$\vec{D} \parallel \vec{E}$$

in an anisotropic medium, $\vec{D} \nparallel \vec{E}$

$$\vec{D} = \vec{E} + 4\pi \vec{P}$$

↑
applied

↑
induced polarization

Due to asymmetry of crystal, $\vec{P} \nparallel \vec{E}$ e.g. 

write $\vec{D} = \vec{\epsilon} \cdot \vec{E}$

$\vec{\epsilon}$ = dielectric tensor = $\begin{pmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{21} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{31} & \epsilon_{32} & \epsilon_{33} \end{pmatrix}$ from thermodynamics, $\vec{\epsilon}$ is symmetric $\epsilon_{ij} = \epsilon_{ji}$

We can choose the orientation of coordinates to diagonalize

$$\rightarrow \begin{pmatrix} P_x \\ P_y \\ P_z \end{pmatrix} = \begin{pmatrix} \epsilon_x & & \\ & \epsilon_y & \\ & & \epsilon_z \end{pmatrix} \begin{pmatrix} E_x \\ E_y \\ E_z \end{pmatrix}$$

this coord. system is aligned along the crystal axes.

so if $\vec{E} = E_x \hat{x} + E_y \hat{y} + E_z \hat{z}$,

$$\vec{D} = P_x \hat{x} = \epsilon_x E_x \text{ only.}$$

biaxial crystal: $\epsilon_x \neq \epsilon_y \neq \epsilon_z$

uniaxial crystal: one pair is the same. e.g. $\epsilon_x = \epsilon_y \neq \epsilon_z$

isotropic crystal $\epsilon_x = \epsilon_y = \epsilon_z = \epsilon$ $\vec{D} = \epsilon \begin{pmatrix} 1 & & \\ & 1 & \\ & & 1 \end{pmatrix} \vec{E}$

The index ellipsoid.

electromagnetic energy density:

$$2 U_E = \frac{\vec{D} \cdot \vec{E}}{4\pi} \quad \text{with } D_x = \epsilon_x E_x, D_y = \epsilon_y E_y, D_z = \epsilon_z E_z \text{ in the crystal axis coord. system.}$$

$$\rightarrow 8\pi U_E = \frac{D_x^2}{\epsilon_x} + \frac{D_y^2}{\epsilon_y} + \frac{D_z^2}{\epsilon_z}$$

$$\frac{1}{8\pi U_E} \left(\frac{D_x^2}{n_x^2} + \frac{D_y^2}{n_y^2} + \frac{D_z^2}{n_z^2} \right) = 1$$

let $\hat{d} = \vec{D} / \sqrt{8\pi U_E}$ be a unit vector for the direction of \vec{D}

then $\frac{d_x^2}{n_x^2} + \frac{d_y^2}{n_y^2} + \frac{d_z^2}{n_z^2} = 1$ eqn. of ellipse.

Normally, we specify $\hat{k} = \frac{\vec{k}}{k_0}$

if \vec{k}, \vec{D} are in $x-z$ plane,

$$n_x = n_o, n_z = n_e$$

$$\vec{k} = \hat{x} k \sin \theta + \hat{z} k \cos \theta$$

with $k = n_e(\theta) k_0$

since $\vec{D} = -\frac{1}{k_0} \vec{E} \times \vec{H}$ and $\vec{H} = \hat{y} H_0$

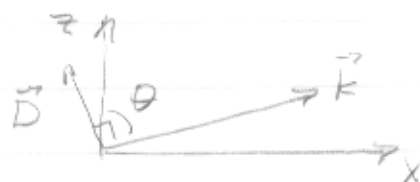
$$= -\frac{1}{k_0} \left(-\hat{x} k_z H_0 + \hat{z} k_x H_0 \right)$$

$$D_x = \frac{k_z}{k_0} H_0 = n_e(\theta) \cos \theta H_0$$

$$D_z = \frac{k_x}{k_0} H_0 = n_e(\theta) \sin \theta H_0$$

$$\rightarrow \frac{H_0^2 / 8\pi}{U_E} n_e^2(\theta) \left(\frac{\sin^2 \theta}{n_e^2} + \frac{\cos^2 \theta}{n_o^2} \right) = 1$$

1 equal energy $U_E = U_H$ (need proof)



• wavelength separation:

- prism: no background, - polarized (too expensive)
- dichroic mirror: typ. refl harmonic at "S" transmit fundam. at "P"



for best efficiency

often need multiple mirrors to get rid of fundam.

• temperature stabilization.

- heating to drive off moisture.
- harmonic is often partly absorbed in crystal

$$\rightarrow \Delta T \rightarrow \Delta k$$

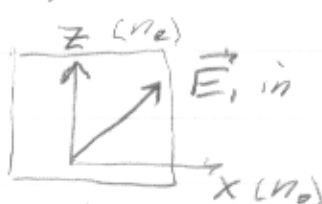
\therefore stabilize at $T \rightarrow T_{room}$.

- can fracture Δk with ΔT

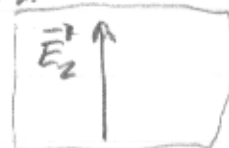
Type II:

- often seen with KTP higher nonlinearity.
- tripling after type I doubling.
- equal \vec{E}_1 along n_o, n_o .

input
 $\vec{k} \otimes$



output



\therefore output at 45° to input.

mirrors out of plane used to flip polarization. (typically)

Angular acceptance:

input beam must be collimated.

divergent beam has a spread of input directions:



doesn't matter much in one direction

in other \rightarrow conversion varies across beam

- see line go across beam.

to calculate:

plot $\text{sinc}^2(\Delta k(\theta_{\text{opt}} + d\theta) L/2)$ vs $d\theta$
some crystals more forgiving

- Type III is best.

Require \sim several mrad, may restrict crystal length

PM bandwidth

- short pulses \rightarrow range $\Delta\omega$

- plot $\text{sinc}^2(\Delta k(\omega_0 + \Delta\omega) L/2)$ vs $\Delta\omega$

want $> 90\%$ across input ^{opt} input BW

- restricts length for short pulses.

Group velocity walk off.

- connected to PM bandwidth

group delay $\tau_g = L/v_g$

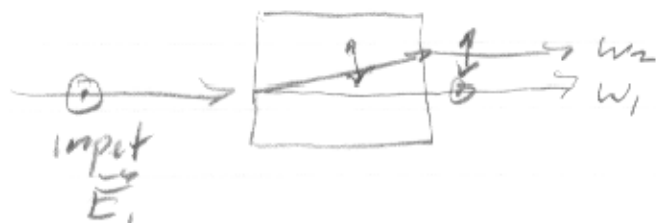
if $|\tau_g(\omega) - \tau_g(2\omega)| > \tau_p$

\rightarrow inefficient doubling.

Beam walk off.

harmonic propagates w/ \vec{k} // crystal axis

→ redirection of power flow



if using small beams (e.g. in focus)

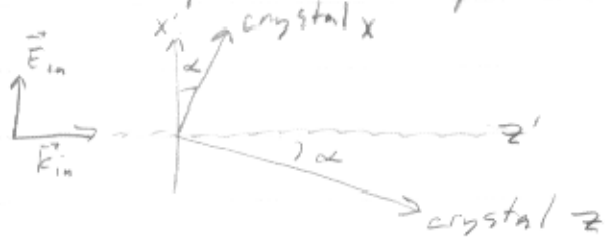
→ power walks off, less efficient

Walkoff

consider plane wave normally incident on surface

- input \vec{E} along \vec{S} outside crystal

- input is at angle to crystal axes:



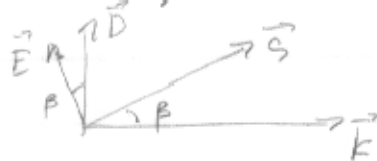
boundary conditions: D^\perp and E^\parallel are continuous.

know that $\vec{E} \parallel \vec{D}$ \therefore one of them bends.

\vec{D}_{in} must be \parallel to \vec{D}_{out}

but $\vec{E}_{out} = E_{in} \hat{x}' + E_{new} \hat{z}'$ is ok.

\therefore inside crystal



beam can refract even at normal inc.

but opposite polarization does not refract if it's along crystal y axis

\rightarrow double image for unpolarized light

two rays walk off from each other \therefore angle β

$$\cos \beta = \frac{\vec{E} \cdot \vec{D}}{E_0 D_0} = \frac{D_x/E_x + D_y/E_y + D_z/E_z}{E_0 D_0}$$

$$\vec{D}_{in} = D_0 \hat{x}' = D_0 \cos \alpha \hat{x} - D_0 \sin \alpha \hat{z} \quad D_y = 0$$

$$\cos \beta = \frac{D_0^2 \left(\frac{\cos^2 \alpha}{E_x} + \frac{\sin^2 \alpha}{E_z} \right)}{D_0^2 \left(\frac{\cos^2 \alpha}{E_x} + \frac{\sin^2 \alpha}{E_z} \right)^{1/2} \left(\cos^2 \alpha + \sin^2 \alpha \right)^{1/2}}$$

$$\text{calculate: } n_x = 1.658 \quad n_z = 1.486 \quad \alpha = 35^\circ \rightarrow \beta = 6.1^\circ$$

Pulse evolution:

Ideally, pulse gets shorter during harmonic generation:

$$E_2(t) \propto E_1^2(t)$$

For gaussian input pulse,

$$E_2(t) \propto E_{i0}^2 \exp(-2t^2/\tau_{p1}^2)$$

→ gaussian, with $\tau_{p2} = \tau_{p1}/\sqrt{2}$

→ corresponding changes in bandwidth.

pulse broadening:

- PM bandwidth
- GV walkoff.

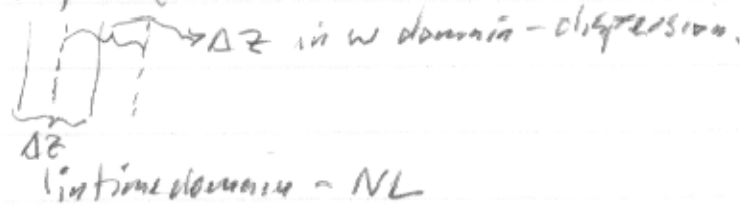
Chirped input?

$|E_1(\omega)|$ unchanged, but $|E_1(t)|$ less

Nonlinearity acts in time domain!

- simulation: split-step method.

Δz split



in time domain - NL