

## Antenna performance.

Hertz

dipole antenna:  $\langle \frac{dP}{d\Omega} \rangle = \frac{1}{2} \frac{\pi}{c} \left( \frac{d}{\lambda} \right)^2 I_0^2 \sin^2 \theta$   
 ( $d \ll \lambda$ )

$\langle P \rangle = \frac{1}{2} \frac{8\pi^2 d^2}{3c} I_0^2$   $\rightarrow$  rad. resistance.

center-fed linear antenna:

$$\langle \frac{dP}{d\Omega} \rangle = \frac{1}{2} \frac{1}{\pi c} \left( \frac{\cos\left(\frac{kd}{2} \cos\theta\right) - \cos\left(\frac{kd}{2}\right)}{\sin\theta} \right)^2 I_0^2$$

this gives the angular distrib. of power.

$$\langle P \rangle_{\text{tot}} = \int_{4\pi} \langle \frac{dP}{d\Omega} \rangle d\Omega$$

how much of the power is directed?

gain  $G \equiv \frac{\langle dP/d\Omega \rangle_{\text{max}}}{P_{\text{tot}}/4\pi}$

if antenna is isotropic - gain = 1

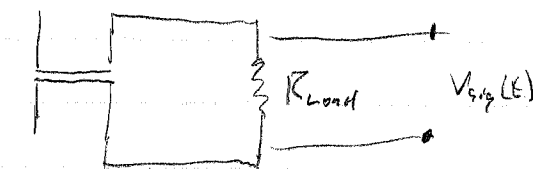
Hertz dipole:  $G = 3/2 = 1.5$

$\lambda/2$  linear  $G = 1.64$

High gain possible for  $d \gg \lambda$  (or use an array)

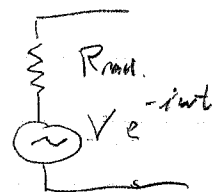
## receivers

EM waves that are broadcast induce currents in rec. antennas.



antenna.

antenna is like a current source  $\rightarrow$



Ideally, match  $R_{rad}$  to  $R_{load}$ .

in this case  $\rightarrow$  maximum power transfer:

$$P_{max} = \frac{E_0^2}{8R_{rad}} \quad (\text{see HW}) \quad E_0 = \text{ind. emf (voltage)}$$

input wave has an intensity  $\langle S \rangle = \frac{\text{power}}{\text{area}}$ .

$$\rightarrow \text{received power is } P_{max} = \langle S \rangle A$$

$\hookrightarrow$  effective area.

$$E_0 = (E_{rad})_{\text{Hertz}} \cdot l = E_{in} l$$

$$\langle S \rangle = \frac{c}{8\pi} E_{in}^2$$

$$\langle P_{max} \rangle = \frac{(E_{in} l)^2}{8R_{rad}} = \frac{c}{8\pi} E_{in}^2 A$$

$$\rightarrow A = \frac{\pi l^2}{c R_{rad}} = \frac{\pi l^2}{c} \frac{3c}{8\pi^2 l} = \frac{3}{8\pi} \lambda^2$$

general antenna:

$$A = G A_0 \quad A_0 = \left( \frac{\lambda}{4\pi} \right)^2$$

communication link

$$P_{\text{out}} = G_r \cdot A_o \cdot S$$

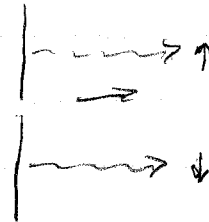
received

$$= G_r \cdot A_o \cdot \frac{G_t \cdot P_{\text{in}}}{4\pi r^2}$$

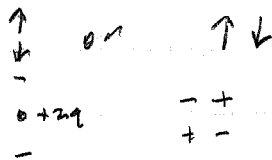
$$\frac{P_{\text{out}}}{P_{\text{in}}} = G_r G_t \cdot \frac{\lambda^2}{4\pi} \cdot \frac{1}{4\pi r^2} = \frac{A_r A_t}{\lambda^2 r^2}$$

Can improve gain by making antenna arrays.

- a small dipole is like a  $\lambda/2$  antenna.
- simulate  $\lambda$  antenna by two small dipoles separated by  $d/2$



can also get radiation from quadrupoles:



or magnetic dipoles

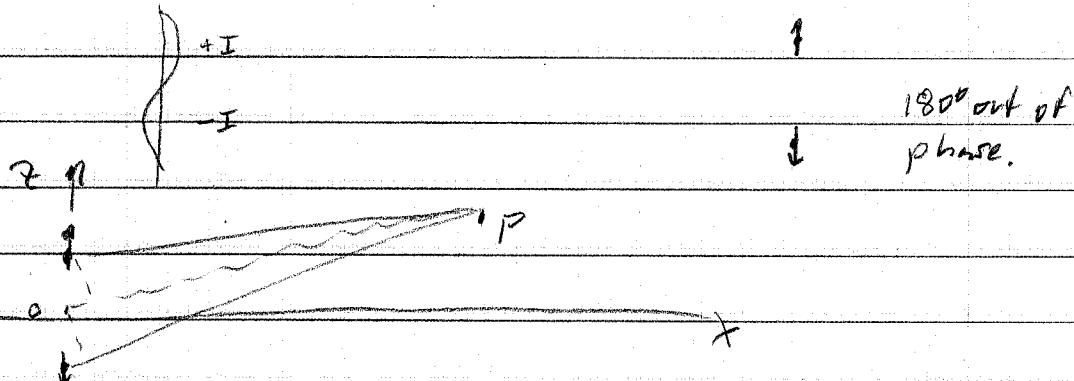


or any other multipole moment.

# Antenna arrays: qualitative picture

Full wave linear antenna

dipole <sup>pair</sup> model

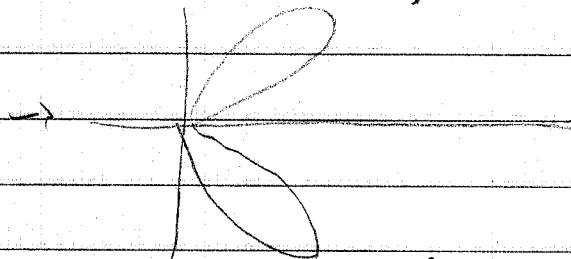


Add E-fields from each dipole

- account for phase delay

where is field  $\rightarrow 0$ ?

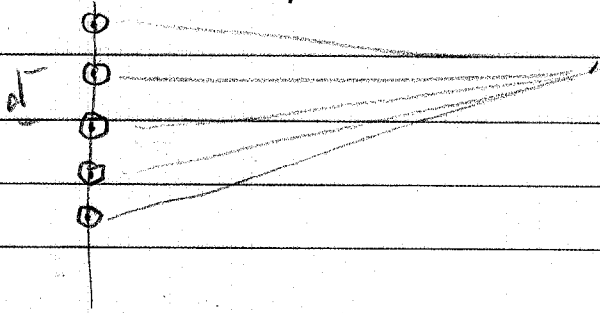
- on-axis b/c dipoles are out of phase.



axial quadrupole

lateral

Extension to arrays:



each dipole has  
ampl. + phase.

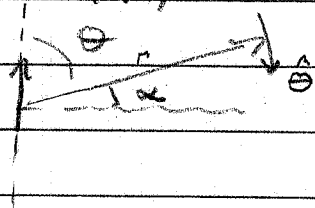
$$m \lambda = d \sin \theta$$

For uniform phase.

## Antenna arrays - dipole modeling

- powerful simulation based on simple ideas

individual dipole radiator:



$$\vec{E}_\alpha = \frac{[\ddot{\vec{p}}]}{c^2 r} \sin^2 \theta \hat{\theta}$$

note polarization is in same orientation as dipole

- linearly polarized, no  $\hat{\phi}$ ,  $\vec{E} \perp \hat{r}$

field is maximum at  $\theta = \pi/2$

> change angle to  $\alpha = \pi/2 - \theta$

$$E_\alpha = \frac{[\ddot{\vec{p}}]}{c^2 r} \cos^2 \alpha$$

$$p(t) = p_0 e^{-i\omega t} \rightarrow \ddot{p} = -\omega^2 p_0 e^{-i\omega t}$$

$$[\ddot{\vec{p}}] = -\omega^2 p_0 e^{-i\omega(t-r/c)}$$

where we are  
evaluating at the  
retarded time.

$$E_\alpha = -\frac{\omega^2}{c^2 r} \cos^2 \alpha e^{i(\frac{\omega r}{c} - \omega t)}$$

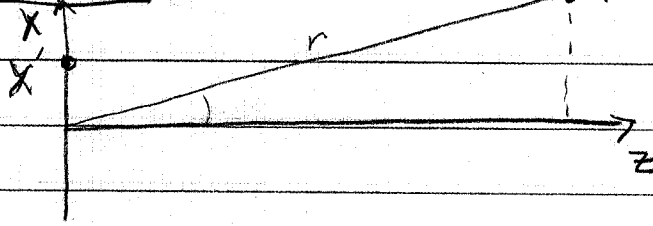
$$\omega/c = k \quad \text{in vacuum. } i(kr - \omega t)$$

$$E_\alpha = -\frac{k^2}{r} \cos^2 \alpha e$$

we'll evaluate it  $t=0$ , drop sign.

$$\vec{P} = P_0 \hat{y}$$

X-Z plane:  $\alpha = 0$



$$r = \sqrt{x^2 + z^2}$$

$$E_y = \frac{P_0 k^2}{r} e^{i k r} \quad \text{with } r \rightarrow \sqrt{x^2 + z^2}$$

add shift:  $x \rightarrow x - x'$

This is form of spherical wave.

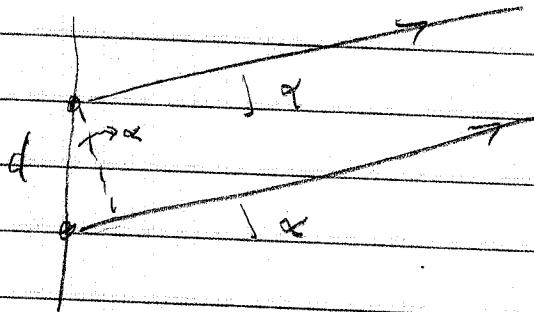
Y-Z plane:  $\cos \alpha = z/r$

$$E_y = E_0 \cos \alpha \rightarrow \frac{P_0 k^2 \cos^2 \alpha}{r} e^{i k r}$$

$$E_z = E_0 \sin \alpha \rightarrow \frac{P_0 k^2 \cos \alpha \sin \alpha}{r} e^{i k r}$$

Far-field pattern: Bragg law

At far field, spherical waves are close to plane waves.



optical path difference is  $d \sin \alpha$

Far field is sum:

$$E \sim \frac{1}{r} \sum_j e^{ik(r + jd \sin \alpha)}$$

$\rightarrow$  max when  $k d \sin \alpha = 2\pi m$

$\rightarrow m \lambda = d \sin \alpha$

Bragg law

Note that constant phase shift among sources  
 $\rightarrow$  angular shift in pattern.

examples: phased array radar  
VLA telescope