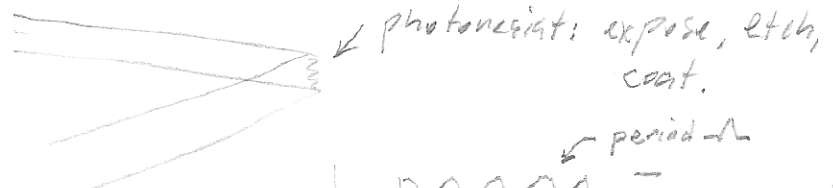


Fraunhofer diffraction: examples + applications.

sinusoidal transmission gratings

- some diffraction gratings are produced by recording interference fringes:



types: absorbing

$$T(x) = \text{rect}(x/d) \left(1 - A + A \cos\left(\frac{2\pi x}{d}\right) \right)$$

phase

$$T(x) = \text{rect}(x/d) \exp(i k_0 n(x) d)$$

$$n(x) = n_0 + n_m \cos\left(\frac{2\pi x}{d}\right)$$

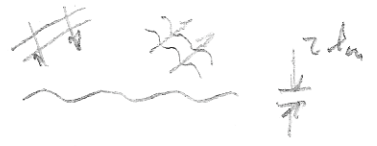
with $k_0 n_m d \ll 1$

$$T(x) \approx \text{rect}(x/d) e^{i k_0 n_0 d} \left(1 + i k_0 n_m d \cos\left(\frac{2\pi x}{d}\right) \right)$$

imag! ↗

reflection = phase

$$R(x) = \text{rect}(x/d) e^{i k_0 n_m d \cos\left(\frac{2\pi x}{d}\right)}$$



In any case, transmission is of the form

$$T(x) = a + b \cos\left(\frac{2\pi x}{d}\right)$$

note that $2\pi/d$ is a type of wavevector. Let $k_{xm} = 2\pi/d$

if incident wave is $e^{i k_0 z}$ wave just past the grating is

$$a e^{i k_0 z} + \frac{1}{2} b \left(e^{i(k_{xm} x + k_0 z)} + e^{i(-k_{xm} x + k_0 z)} \right)$$

sum of 3 waves:

$$\sim e^{i(k_{xm} x + k_0 z)} \quad (+1 \text{ order})$$



$$\sim e^{i k_0 z} \quad (\text{zero order})$$

$$\sim e^{i(-k_{xm} x + k_0 z)} \quad (-1 \text{ order})$$

k_{xm} is a spatial frequency $= k_0 \sin \theta_m$
 plane wave traveling at angle θ_m

Side note: outgoing wave really should be of the form

$$\exp(i k_0 (x \sin \theta_m + z \cos \theta_m))$$

to conserve \vec{k} (which is like photon momentum, $\hbar \vec{k}$)

But we are implicitly looking at small angles: $\cos \theta_m \approx 1$.

Do diff. integral:

$$E_{diff}(X, Y) = \frac{e^{i k_0 R}}{i \lambda R} \iint_{-\infty}^{\infty} E_{in}(x, y) T(x, y) e^{-i \left(\frac{k_0 X}{R} x + \frac{k_0 Y}{R} y \right)} dx dy$$

or

$$= \frac{e^{i k_0 R}}{i \lambda R} \mathcal{F}_{xy} \{ E_{in}(x, y) T(x, y) \} \quad \text{with } \beta_x = \frac{k_0 X}{R}$$

$$\beta_y = \frac{k_0 Y}{R}$$

Here $E_{in}(x, y) = E_0$ at $z=0$

$$T(x, y) = \text{rect}(x/D) (a + b \cos(k_m x)) \text{rect}(y/D)$$

for a square grating.

$$= T_x(x) T_y(y)$$

$$E_{diff}(X, Y) = \frac{e^{i k_0 R}}{i \lambda R} \mathcal{F}_x \{ T_x(x) \} \mathcal{F}_y \{ T_y(y) \}$$

notice $T(x, y)$ is separable, no convolution because x, y are different spaces.

$$E_{diff}(X, Y) = \frac{e^{i k_0 R}}{i \lambda R} \left(\frac{D}{2\pi} \text{sinc}\left(\frac{\beta_x D}{2}\right) \otimes \left(a 2\pi \delta(\beta_x) + \frac{b}{2} 2\pi (\delta(\beta_x + k_m) + \delta(\beta_x - k_m)) \right) \right) \cdot \left(D \text{sinc}\left(\frac{\beta_y D}{2}\right) \right)$$

recall that β_x variable is like $k_0 \sin \theta_x = \frac{k_0 X}{R}$
 so physical meaning of $\delta(\beta_x + k_{mx})$ is that the
 wave has a well-defined angle:

$$k_0 \sin \theta_x + k_{mx} = 0 \quad \text{at} \quad \sin \theta_x = -\frac{k_{mx}}{k_0}$$

$$\text{or} \quad \sin \theta_x = -\frac{\frac{2\pi}{\lambda} \frac{d}{2}}{\frac{2\pi}{\lambda}} = (-1) \lambda/d \quad \text{like grating eqn.}$$

carry out convolution:

$$E_{diff}(X, Y) = \frac{e^{ikR}}{i\lambda R} D^2 \left[a \operatorname{sinc}\left(\frac{\beta_x D}{2}\right) + \frac{b}{2} \left(\operatorname{sinc}\left(\frac{\beta_x + k_{mx}}{2} D\right) + \operatorname{sinc}\left(\frac{\beta_x - k_{mx}}{2} D\right) \right) \right] \operatorname{sinc}\left(\frac{\beta_y D}{2}\right)$$

We can separate out the physical effects of the grating,
 which splits beam into diff orders (angles) and the
 aperture of the grating, which \rightarrow $\operatorname{sinc}()$ envelope.

Add lens: $\beta_x = \frac{k_0 X}{R} \rightarrow \frac{k_0 X}{f}$

in focal plane, measure intensity: $|E_{diff}|^2$

- if peaks are separate, cross terms aren't imp.

e.g. $\operatorname{sinc}\left(\frac{\beta_x D}{2}\right) \operatorname{sinc}\left(\frac{(\beta_x + k_{mx}) D}{2}\right) \approx 0$

