

NLO with guided waves.

1) solve linear eqn for transverse mode structure.

$$\nabla_T^2 A + (k_0^2 n^2(r) - k_z^2) A = 0 \quad \text{assume azimuthal symmetry.}$$

modal solutions $U_m(r)$

$$A(r, z, t) = \sum_m a_m U_m(r) e^{i(k_{zm} z - \omega t)}$$

- each mode has its own propagation constant.
- if all light is guided $\rightarrow U_m$ is a complete set
- otherwise there are unguided waves too (radiation modes)
- a_m = amplitude coeff. Constant if linear, no loss.

2) calculate NL polarization e.g. $\chi^{(3)}$ THG

$$P^{NL} \propto \chi^{(3)} A^3 \quad \text{picking out } \omega_3 = 3\omega_1$$

easiest if input is all same mode

$$P^{NL} \sim a_{1m}^3(z) U_{1m}^3(r) e^{i 3k_{1m} z}$$

3) project P^{NL} onto guided modes for $\omega_3 = 3\omega_1$.

separate eqns for $a_{3m}(z)$

$$2i k_{3m} \frac{da_{3m}}{dz} e^{i k_{3m} z} \propto k_{1m}^2 \chi^{(3)} a_{1m}^3 e^{i 3k_{1m} z} \cdot \underbrace{2\pi \int_0^\infty U_{3m}^*(r) U_{1m}^3(r) r dr}_{\text{mode overlap}}$$

\rightarrow lower effective $\chi^{(3)}$

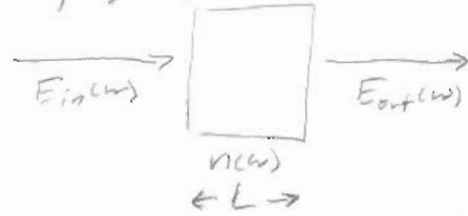
note phase matching is mode-selective.

$$\Delta k = 3k_{1m} - k_{3m}$$

can use modes to assist phase matching.

Time vs. Frequency domain

Linear response:



$$E_{out}(w) = E_{in}(w) e^{i k_0 n(w) L}$$

Linear propagation is easiest to describe in freq. space.

- linear systems: $H(w) =$ transfer fun, freq. response

$$F_{out}(w) = H(w) F_{in}(w)$$

$$F_{out}(t) = \mathcal{F}^{-1} \{ H(w) F_{in}(w) \}$$

$$= h(t) \otimes f_{in}(t)$$

where $= \int_{-\infty}^{\infty} h(\tau) f_{in}(t-\tau) d\tau$ is convolution. convolution theorem

if input is $f_{in}(t) = \delta(t)$ (impulse)

$$F_{out}(t) = \int_{-\infty}^{\infty} h(\tau) \delta(t-\tau) d\tau = h(t)$$

$\therefore h(t) = \mathcal{F}^{-1} \{ H(w) \}$ is impulse response.

At a microscopic level, $p(t)$ is the induced dipole when $E(t)$ is in and $P(t) = N_a p(t)$ is the collective response.

When we solve for $\chi''' = N_a P/E$, our method gives $\chi'''(w)$

recall steps: $E(t) = E_0 e^{-i\omega t} + c.c.$

$$x'''(t) = x_0''' e^{-i\omega t} + c.c.$$

$$x_0''' = -(e/m) E_0 / D(\omega)$$

$$\chi'''(\omega) = N_a e^2 / m / D(\omega)$$

So what is the impulse response? For a range of input freq:

$$P''(\omega) = X''(\omega) E(\omega)$$

Alternative method: take FT of 2nd order eqn.

note that $\mathcal{F}\left\{\frac{d}{dt}\right\} = -i\omega F(\omega)$
 \rightarrow eqn for $X''(\omega)$ with $E(\omega)$ driving

Now in time domain,

$$P''(t) = \mathcal{F}^{-1}\{X''(\omega) E(\omega)\}$$

Recognize $X''(\omega)$ as a transfer function.

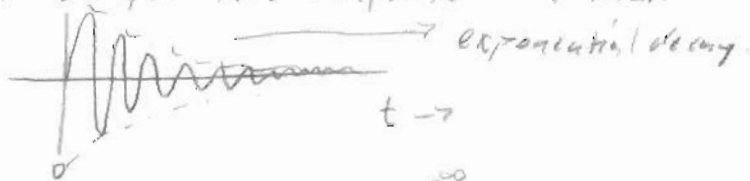
let $R''(t) \equiv \mathcal{F}^{-1}\{X''(\omega)\} \equiv$ impulse response

$$\text{Then } P''(t) = \epsilon_0 \int_{-\infty}^{\infty} R''(\tau) E(t-\tau) d\tau = R'' \otimes E$$

(normally have $\frac{1}{2\pi}$ in front, this is absorbed into def'n of R)

What is the nature of $R''(t)$?

- causality requires $R''(t) = 0$ for $t < 0$
- expect? damped SHD response to a kick:



$$\text{- Proof: } \mathcal{F}^{-1}\{X''(\omega)\} = \frac{1}{2\pi} \int_{-\infty}^{\infty} \frac{N(\omega'/\omega_0)}{\omega_0^2 - \omega'^2 - 2i\omega'\delta} e^{-i\omega't} d\omega'$$

requires contour integration: poles are off real axis:



for $t < 0$ close on upper half $\rightarrow 0$
 for $t > 0$ close lower.